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Transmission media and optical systems characteristics — Optical fibre cables

Definitions and test methods for linear, deterministic attributes of single-mode fibre and cable

Recommendation T G.650.1

Recommendation ITU-T G.650.1

Definitions and test methods for linear, deterministic attributes of single-mode fibre and cable

Summary

Recommendation ITU-T G.650.1 contains definitions of the linear, deterministic parameters of single-mode optical fibres and cables. It also contains both reference test methods and alternative test methods for characterizing these parameters.

These test methods are suitable mainly for factory measurements of the linear, deterministic attributes of single-mode fibres and cables. Some of the test methods may also be used to characterize discrete optical components.

The history of this Recommendation is as follows:

1993 Definitions and test methods were removed from single-mode fibre Recommendations such as Recommendation [ITU-T G.652] and used to create the initial version of Recommendation ITU-T G.650.

1997 The second version of Recommendation ITU-T G.650 added definitions and test methods for polarization mode dispersion and appendices I, II and III. The improved determination of cut-off wavelength (clause 5.3.1.3.4) was also added.

2000 The third version established reference and alternative test methods for polarization mode dispersion, modified the definitions and test methods for core concentricity error (clauses 3.4 and 5.2), and added clause 5.1.4 and appendices IV, V and VI.

2002 In order to facilitate maintenance, Recommendation ITU-T G.650 was divided into smaller Recommendations. Recommendation ITU-T G.650.2 contains definitions and test methods for statistical and non-linear attributes of single-mode fibre and cable.

2004 The second version of Recommendation ITU-TG.650.1 added a third alternative test method "Spectral attenuation modelling" (clause 5.4.4) and new Appendix III "Example of a matrix model". This material has been moved from the single-mode fibre Recommendations into this Recommendation ITU-T G.650.1. In addition, chromatic dispersion fitting procedures have been added (Annex A).

2010 The third version of Recommendation ITU-TG.650.1 added the test method "Test methods for the macrobend loss" (clause 5.6). Jumper cut-off wavelength has been deleted from clause 5.3. An additional description has been added in cut-off wavelength test method (clause 5.3.1.3.2). Equation 5-1 has been corrected. A detailed description has been added in proof test method (clause 5.7). Appendix II has been updated.

2018 The fourth version of Recommendation ITU-TG.650.1 added Appendix IV (from Amendment 1 published in 2012) to provide measurement procedures for coherent multipath interference (MPI). The interferometric technique for chromatic dispersion measurement has been deleted from clause 6.5 and moved to Appendix V. The description of measurement details for [ITU-T G.657] fibre on MFD, cut-off wavelength and spectral attenuation tests has been improved. The RTM and ATM of cable cut-off wavelength measurement has been modified. An example of the interpolation method has been added in clause I.3. Equation 6-1 has been corrected.

History

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Keywords

Deterministic attributes, linear attributes, single-mode fibre characterization.

FOREWORD

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The World Telecommunication Standardization Assembly (WTSA), which meets every four years, establishes the topics for study by the ITU T study groups which, in turn, produce Recommendations on these topics.

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Recommendation ITU-T G.650.1

Definitions and test methods for linear, deterministic attributes of single-mode fibre and cable

1. Scope

This Recommendation contains definitions and test methods suitable mainly for factory measurements of the linear, deterministic attributes of the single-mode optical fibres and cables described in [ITU-T G.652], [ITU-T G.653], [ITU-T G.654], [ITU-T G.655], [ITU-T G.656] and [ITU-T G.657]. These definitions and test methods are generally not appropriate for multimode fibre, such as that specified in [ITU-T G.651.1]. Some of the test methods, when so indicated, may also be used to characterize discrete optical components, such as those described in [ITU-T G.671]. [ITU-T G.650.2] contains definitions and test methods for statistical and non-linear attributes.

2. References

The following ITU-T Recommendations and other references contain provisions which, through reference in this text, constitute provisions of this Recommendation. At the time of publication, the editions indicated were valid. All Recommendations and other references are subject to revision; users of this Recommendation are therefore encouraged to investigate the possibility of applying the most recent edition of the Recommendations and other references listed below. A list of the currently valid ITU-T Recommendations is regularly published. The reference to a document within this Recommendation does not give it, as a stand-alone document, the status of a Recommendation.

[ITU-T G.650.2]*Definitions and test methods for statistical and non-linear related attributes of single-mode fibre and cable*, 7th edition.

[ITU-T G.651.1]*Characteristics of a 50/125 µm multimode graded index optical fibre cable for the optical access network*, 2nd edition.

[ITU-T G.652]*Characteristics of a single-mode optical fibre and cable*, 9th edition.

[ITU-T G.653]*Characteristics of a dispersion-shifted, single-mode optical fibre and cable*, 7th edition.

[ITU-T G.654]*Characteristics of a cut-off shifted single-mode optical fibre and cable*, 11th edition.

[ITU-T G.655]*Characteristics of a non-zero dispersion-shifted single-mode optical fibre and cable*, 5th edition.

[ITU-T G.656]*Characteristics of a fibre and cable with non-zero dispersion for wideband optical transport*, 3rd edition.

[ITU-T G.657]*Characteristics of a bending-loss insensitive single-mode optical fibre and cable*, 4th edition.

[ITU-T G.671]*Transmission characteristics of optical components and subsystems*, 7th edition.

[IEC 60793-1-1 RLV]*Optical fibres — Part 1-1: Measurement methods and test procedures — General and guidance*, 5.0.

[IEC 60793-1-30]*Optical fibres — Part 1-30: Measurement methods and test procedures — Fibre proof test*, 2.0.

[IEC 60793-1-42]*Optical fibres — Part 1-42: Measurement methods and test procedures — Chromatic dispersion*, 3.0.

[IEC 60793-1-44]*Optical fibres — Part 1-44: Measurement methods and test procedures — Cut-off wavelength*, 2.0.

[IEC 60793-1-45 RLV]*Optical fibres — Part 1-45: Measurement methods and test procedures — Mode field diameter*, 2.0.

[IEC 60793-1-46]*Optical fibres — Part 1-46: Measurement methods and test procedures — Monitoring of changes in optical transmittance*, 1.0.

[IEC 60793-1-47 RLV]*Optical fibres — Part 1-47: Measurement methods and test procedures — Macrobending loss*, 4.0.

[IEC 61745]*End-face image analysis procedure for the calibration of optical fibre geometry test sets*, 2.0.

[IEC 61746-1]*Calibration of optical time-domain reflectometers (OTDR) — Part 1: OTDR for single mode fibres*, 1.0.

3. Definitions

This Recommendation defines the following terms:

3.1. General definitions

3.1.1. alternative test method (ATM): A test method in which a given characteristic of a specified class of optical fibres or optical fibre cables is measured in a manner consistent with the definition of this characteristic and gives results which are reproducible and relatable to the reference test method and to practical use.

3.1.2. cladding mode stripper: A device that encourages the conversion of cladding modes to radiation modes.

3.1.3. mode filter: A device designed to accept or reject a certain mode or modes.

3.1.4. reference test method (RTM): A test method in which a characteristic of a specified class of optical fibres or optical fibre cables is measured strictly according to the definition of this characteristic and which gives results which are accurate, reproducible and relatable to practical use.

3.1.5. refractive index profile: The refractive index along a diameter of the fibre.

3.2. Mechanical characteristics

3.2.1. proof test level: The proof test level is the specified value of tensile stress or strain to which a full length of fibre is subjected for a specified short time period. This isusually done sequentially along the fibre length.

3.2.2. stress corrosion parameter: The stress corrosion (susceptibility) parameter n is a dimensionless coefficient empirically related to the dependence of crack growth on applied stress. It depends upon the ambient temperature, humidity and other environmental conditions.

Both a static and a dynamic value for this parameter can be given.

The static value n_s is the negative of the slope of a static fatigue log-log plot of failure time versus applied stress.

The dynamic value is n_d where $1/(n_d + 1)$ is the slope of a dynamic fatigue log-log plot of failure stress versus applied stress rate.

NOTE – n need not be an integer.

3.3. Glass geometry characteristics

3.3.1. cladding: The outermost region of glass in the fibre cross section.

3.3.2. cladding centre: The centre of a circle which best fits the cladding boundary.

NOTE – The method of bestfitting has to be specified.

3.3.3. cladding diameter: The diameter of the circle defining the cladding centre.

3.3.4. cladding diameter deviation: The difference between the actual and the nominal values of the cladding diameter.

3.3.5. cladding non-circularity: The difference between the diameters of the two circles defined by the cladding tolerance field, divided by the cladding diameter.

3.3.6. cladding tolerance field: For a cross section of an optical fibre, it is the region between the circle circumscribing the outer limit of the cladding, and the largest circle, concentric with the first one, that fits into the outer limit of the cladding. Both circles shall have the same centre as the cladding.

3.3.7. core centre: The core centre is the centre of a circle which best fits the points at a constant level in the near-field intensity pattern emitted from the central region of the fibre, using wavelengths above and/or below the fibre's cut-off wavelength.

NOTE 1 – The above constant level shall be chosen between 5% and 50% of maximum near-field intensity.

NOTE 2 – Usually, the core centre represents a good approximation of the mode field centre.

3.3.8. core concentricity error: The distance between the core centre and the cladding centre.

3.4. Optical characteristics

3.4.1. mode field definitions

3.4.1.1. mode field: The mode field is the single-mode field distribution of the LP_{01} mode giving rise to a spatial intensity distribution in the fibre.

3.4.1.2. mode field centre: The mode field centre is the position of the centroid of the spatial intensity distribution in the fibre.

$$r_c = \frac{\iint_{Area} rI(r)\,dA}{\iint_{Area} I(r)\,dA} \quad (3\text{-}1)$$

NOTE 1 – The centroid is located at r_c and is the normalized intensity-weighted integral of the position vector r.

NOTE 2 – The correspondence between the position of the centroid, as defined, and the position of the maximum of the spatial intensity distribution requires further study.

3.4.1.3. mode field concentricity error: The distance between the mode field centre and the cladding centre.

3.4.1.4. mode field diameter: The mode field diameter (MFD) $2w$ represents a measure of the transverse extent of the electromagnetic field intensity of the mode in a fibre cross section, and it is defined from the far-field intensity distribution $F^2(\theta)$, θ being the far-field angle, through the following equation:

$$2w = \frac{\lambda}{\pi}\left[\frac{2\int_0^{\frac{\pi}{2}} F^2(\theta)\sin\theta\cos\theta d\theta}{\int_0^{\frac{\pi}{2}} F^2(\theta)\sin^3\theta\cos\theta d\theta}\right]^{\frac{1}{2}} \tag{3-2}$$

3.4.1.5. mode field non-circularity: Since it is not normally necessary to measure mode field non-circularity for acceptance purposes, a definition of mode field non-circularity is not necessary in this context.

3.4.2. chromatic dispersion definitions

3.4.2.1. chromatic dispersion: The spreading of alight pulse in an optical fibre caused by the different group velocities of the different wavelengths composing the source spectrum.

3.4.2.2. chromatic dispersion coefficient: Change of the group delay of a light pulse for a unit fibre length caused by a unit wavelength change. Thus, the chromatic dispersion coefficient is $D(\lambda)= d\tau/d\lambda$. It is usually expressed in ps/(nm × km).

3.4.2.3. chromatic dispersion slope: The slope of the chromatic dispersion coefficient versus wavelength curve. The dispersion slope is defined as $S(\lambda) = dD/d\lambda$.

3.4.2.4. group delay: The time required for a light pulse to travel a unit length of fibre. The group delay as a function of wavelength is denoted by $\tau(\lambda)$. It is usually expressed in ps/km.

3.4.2.5. longitudinal uniformity of chromatic dispersion: Change in the chromatic dispersion coefficient over the length of an optical fibre or cable.

3.4.2.6. zero-dispersion slope: The chromatic dispersion slope at the zero-dispersion wavelength.

3.4.2.7. zero-dispersion wavelength: The wavelength at which the chromatic dispersion vanishes.

3.4.3. cut-off wavelength: Theoretical cut-off wavelength is the shortest wavelength at which a single mode can propagate in a single-mode fibre. This parameter can be computed from the refractive index profile of the fibre. At wavelengths below the theoretical cut-off wavelength several modes propagate and the fibre is no longer single-mode but multimode.

In optical fibres, the change from multimode to single-mode behaviour does not occur at an isolated wavelength, but rather smoothly over a range of wavelengths. Consequently, for determining fibre performance in a telecommunication network, theoretical cut-off wavelength is less useful than the actual threshold wavelength for single-mode performance when the fibre is in operation. Thus, a more effective parameter called cut-off wavelength shall be introduced for single-mode fibre specifications as defined in the following:

Cut-off wavelength is defined as the wavelength greater than which the ratio between the total power, including launched higher order modes, and the fundamental mode power has decreased to less than 0.1 dB. According to this definition, the second order (LP_{11}) mode undergoes 19.3 dB more attenuation than the fundamental (LP_{01}) mode when the modes are equally excited.

Because cut-off wavelength depends on the length and bends of the fibre, as well as its strain condition, the resulting value of cut-off wavelength depends on whether the measured fibre is configured in a deployed cabled condition, or whether the fibre is short and uncabled. Consequently, there are two types of cut-off wavelength defined: cable cut-off wavelength and fibre cut-off wavelength.

cable cut-off wavelength λ_{cc}—Cable cut-off wavelength is measured prior to installation on a substantially straight 22 m cable length prepared by exposing 1m of primary-coated fibre at either end, the exposed ends each incorporating a 40 mm radius loop. Alternatively, this parameter may be measured on 22 m of primary-coated uncabled fibre loosely constrained in loops > 140 mm radius, incorporating a 40 mm radius loop at either end.

fibre cut-off wavelength λ_c – Fibre cut-off wavelength is measured on a short length of uncabled, primary-coated fibre.

To avoid modal noise and dispersion penalties, the cut-off wavelength λ_{cc} of the shortest cable length (including repair lengths when present) should be less than the lowest anticipated system wavelength, λ_s:

$$\lambda_{cc} < \lambda_s \quad (3\text{-}3)$$

This ensures that each individual cable section is sufficiently single mode. Any joint that is not perfect will create some higher order (LP_{11}) mode power, and single-mode fibres typically support this mode for a short distance (of the order of metres, depending on the deployment conditions). A minimum distance must therefore be specified between joints in order to give the fibre sufficient distance to attenuate the LP_{11} mode before it reaches the next joint. If Inequality (3-3) is satisfied in the shortest cable section, it will be automatically satisfied in all longer cable sections, and single-mode system operation will occur regardless of the elementary section length.

Fibre cut-off wavelength and mode field diameter can be combined to estimate a fibre's bend sensitivity. High fibre cut-off and a small mode field diameter result in a more bend-resistant fibre. This explains why it is often desirable to specify higher values of cut-off wavelength λ_c, even if the upper limit of this parameter exceeds the operating wavelength. All practical installation techniques and cable designs will ensure a cable cut-off wavelength below the operating wavelength.

Since specification of cable cut-off wavelength, λ_{cc}, is a more direct way of ensuring single-mode cable operation, specifying this is preferred to specifying fibre cut-off wavelength, λ_c. However, when circumstances do not readily permit the specification of λ_{cc} (e.g., in single-fibre cable such as pigtails, jumpers or cables to be deployed in a significantly different manner than in the λ_{cc} RTM), then specifying an upper limit for λ_c is appropriate. This option is addressed in [ITU-T G.652], [ITU-T G.653], [ITU-T G.654], [ITU-T G.655], [ITU-T G.656] and [ITU-T G.657].

NOTE – The single-mode operability of a short (typically less than 10 m) optical fibre can be additionally investigated by evaluating the multipath interference (MPI). General information on MPI is provided in [b-ITU-T G.Suppl.47], Clause 6.1 and coherent MPI test methods are described in Appendix IV of this Recommendation.

3.4.4. attenuation: The attenuation $A(\lambda)$ at wavelength λ between two cross sections 1 and 2 separated by distance L of a fibre is defined as:

$$A(\lambda) = 10\log\frac{P_1(\lambda)}{P_2(\lambda)}\,(dB) \quad (3\text{-}4)$$

where $P_1(\lambda)$ is the optical power traversing cross section 1, and $P_2(\lambda)$ is the optical power traversing cross section 2 at the wavelength λ.

For a uniform fibre, it is possible to define an attenuation per unit length or an attenuation coefficient, which is independent of the length of the fibre:

$$a(\lambda) = \frac{A(\lambda)}{L}\,(\text{dB/unit length})\Big) \quad (3\text{-}5)$$

3.4.5. macrobending loss: The macrobending loss is the loss values under different bend radii, number of coils and wavelengths to evaluate the macrobending performance of optical fibres. The results are reported in dB as:

$$Loss(dB) = 10\log_{10}\frac{P_{str}}{P_{bend}} \quad (3\text{-}6)$$

where P_{str} is the power measured without the bend and P_{bend} is the power measured with the bend present.

3.5. Others

3.5.1. primary coating: The one or more layers of protective coating material applied to the fibre cladding during or after the drawing process to preserve the integrity of the cladding surface and to give a minimum amount of required protection (e.g., a 250 µm protective coating).

3.5.2. secondary coating: The one or more layers of coating material applied over one or more primary-coated fibres in order to give additional required protection or to arrange fibres together in a particular structure (e.g., a 900 µm "buffer" coating, "tight jacket", or a ribbon coating).

4. Abbreviations and acronyms

This Recommendation uses the following abbreviations:

ATM	Alternative Test Method
CCD	Charge Coupled Device
DGD	Differential Group Delay
DWDM	Dense Wavelength Division Multiplexing
ECL	External Cavity Laser
EELED	Edge Emitting Light Emitting Diode
FS	Fibre Stretching
FSR	Free Spectral Range
FWHM	Full Width at Half Maximum
HOM	High-Order Mode
LD	Laser Diode
LED	Light Emitting Diode
MFCE	Mode Field Concentricity Error
MFD	Mode Field Diameter
MPI	Multipath Interference
NA	Numerical Apertures
Nd YAG	Neodymium-doped Yttrium Aluminium Garnet
NFP	Near-Field Pattern
OSA	Optical Spectrum Analyser
OTDR	Optical Time Domain Reflectometer
PM	Power Meter
RIN	Relative Intensity Noise
RTM	Reference Test Method
TBD	To Be Determined
TEM	Transverse Electromagnetic Mode

WDM	Wavelength Division Multiplexing
WTL	Wavelength Tunable Laser

5. Conventions

Unless otherwise specified, use standard range of atmospheric conditions as per [IEC 60793-1-1 RLV].

6. Test methods

Both reference test method (RTM) and alternative test methods (ATMs) are usually given here for each parameter, and it is the intention that both the RTM and the ATM(s) may be suitable for normal product acceptance purposes. However, when using an ATM, should any discrepancy arise, it is recommended that the RTM be employed as the technique for providing the definitive measurement results.

NOTE – The apparatus and procedure given cover only the essential basic features of the test methods. It is assumed that the detailed instrumentation will incorporate all necessary measures to ensure stability, noise elimination, signal-to-noise ratio, etc.

6.1. Test methods for the mode field diameter

6.1.1. Reference test method: The far-field scan

6.1.1.1. General

The mode field diameter is determined from the far-field intensity distribution $F^2(\theta)$, according to the definition given in clause 3.4.1.4. The integration limits are shown to be 0 and $\pi/2$, but it is understood that this notation implies the truncation of the integrals in the limit of increasing argument. While the maximum physical value of the argument θ is $\pi/2$, the integrands rapidly approach zero before this value is reached. The relative error in the determination of the mode field diameter, introduced by this truncation, is discussed in clause 6.1.1.2.6.

6.1.1.2. Test apparatus

A schematic diagram of the test apparatus is shown in Figure 1.

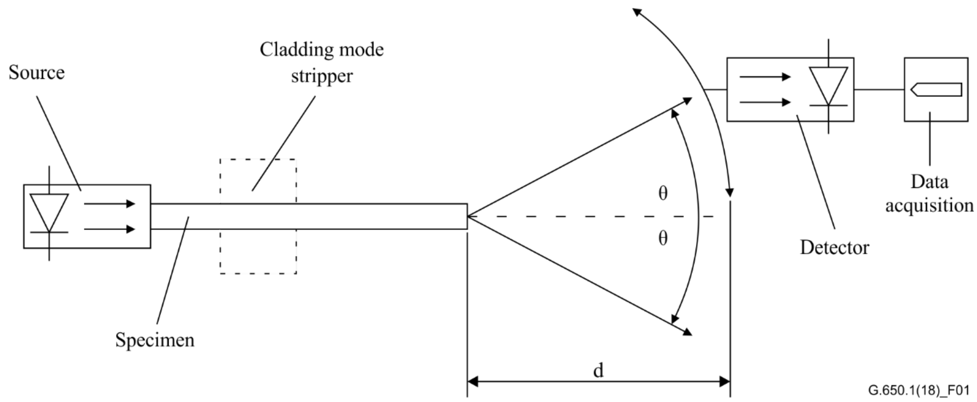


Figure 1 — Typical arrangement of the far-field scan set-up

6.1.1.2.1. Light source

The light source shall be stable in position, intensity and wavelength over a time period sufficiently long to complete the measurement procedure. The spectral characteristics of the source should be chosen to preclude multimode operation. The FWHM spectral width shall be no greater than 10 nm.

6.1.1.2.2. Modulation

It is customary to modulate the light source in order to improve the signal/noise ratio at the receiver. If such a procedure is adopted, the detector should be linked to a signal processing system synchronous with the source modulation frequency. The detecting system should have substantially linear sensitivity characteristics.

6.1.1.2.3. Launching conditions

The launching conditions used must be sufficient to excite the fundamental (LP_{01}) mode. For example, suitable launching techniques could be:

a) jointing with a fibre;

b) launching with a suitable system of optics.

Care should be taken that higher order modes do not propagate. For this purpose, it may be necessary to introduce a loop of suitable radius or another mode filter in order to remove higher order modes. For example, a one-turn bend with a radius of 30 mm on the fibre is generally sufficient for most ITU-T G.65x fibres. For some [ITU-T G.657] fibres, smaller radius, multiple bends or longer sample lengths can be applied to remove high-order propagating modes.

6.1.1.2.4. Cladding mode stripper

Precautions shall be taken to prevent the propagation and detection of cladding modes.

6.1.1.2.5. Specimen

The specimen shall be a short length of the optical fibre to be measured. Primary fibre coating shall be removed from the section of the fibre inserted in the mode stripper, if used. The fibre ends shall be clean, smooth and perpendicular to the fibre axes. It is recommended that the end faces be flat and perpendicular to the fibre axes to within 1°.

6.1.1.2.6. Scan apparatus

A mechanism to scan the far-field intensity distribution shall be used (for example, a scanning photodetector with pinhole aperture or a scanning pig-tailed photodetector). The detector should be at least 10 mm from the fibre end, and the detector's active area should not subtend too large an angle in the far field. This can be assured by placing the detector at a distance from the fibre end greater than 40 wb/λ, where $2w$ is the expected mode field diameter of the fibre to be measured and b is the diameter of the active area of the detector.

The minimum dynamic range of the measurement should be 50 dB. This corresponds to a maximum scan half-angle of 20° and 25°, or greater, for fibres covered by [ITU-T G.652] and [ITU-T G.653], respectively.

NOTE 1 – Reducing such dynamic range (or maximum scan half-angle) requirements may introduce errors. For example, restricting those values to 30 dB and 12.5° for [ITU-T G.652] fibres, and to 40 dB and 20° for [ITU-T G.653] fibres, may result in a relative error, in the determination of the MFD, greater than 1%.

NOTE 2 – For [ITU-T G.654] fibres, the same considerations as for [ITU-T G.652] fibres apply.

6.1.1.2.7. Detector

A suitable detector shall be used. The detector must have linear sensitivity characteristics.

6.1.1.2.8. Amplifier

An amplifier should be employed in order to increase the signal level.

6.1.1.2.9. Data acquisition

The measured signal level shall be recorded and suitably processed.

6.1.1.3. Measurement procedure

The launch end of the fibre shall be aligned with the launch beam, and the output end of the fibre shall be aligned to the appropriate output device.

The following procedure shall be followed: by scanning the detector in fixed steps no greater than 0.5°, the far-field intensity distribution, $F^2(\theta)$, is measured, and the mode field diameter is calculated from Equation (3-2).

6.1.1.4. Presentation of the results

The following details shall be presented:

a) test set-up arrangement, dynamic range of the measurement system, processing algorithms, and a description of the scanning device used (including the scan angle);
b) launching conditions;
c) wavelength and spectral line-width FWHM of the source;
d) fibre identification and length;
e) type of claddingmode stripper;
f) description of high-order modes filter;
g) type and dimensions of the detector;
h) temperature of the sample and environmental conditions (when necessary);
i) indication of the accuracy and repeatability;
j) mode field diameter.

6.1.2. First alternative test method: The variable aperture technique

6.1.2.1. General

The mode field diameter is determined from the complementary aperture transmission function a(x), (x = D·tan θ being the aperture radius, and D the distance between the aperture and the fibre):

$$2w = (\lambda/\pi D)\left[\int_0^\infty a(x)\frac{x}{(x^2+D^2)^2}\mathrm{d}x\right]^{-\frac{1}{2}} \tag{6-1}$$

The mathematical equivalence of Equation (3-2) and Equation (6-1) is valid in the approximation of small angles θ. Under this approximation, Equation (6-1) can be derived from Equation (3-2) by integration.

6.1.2.2. Test apparatus

6.1.2.2.1. Light source (as in clause 6.1.1.2.1)

6.1.2.2.2. Modulation (as in clause 6.1.1.2.2)

6.1.2.2.3. Launching conditions (as in clause 6.1.1.2.3)

6.1.2.2.4. Cladding mode stripper (as in clause 6.1.1.2.4)

6.1.2.2.5. Specimen (as in clause 6.1.1.2.5)

6.1.2.2.6. Aperture apparatus

A mechanism containing at least twelve apertures spanning the half-angle range of numerical apertures from 0.02 to 0.25 (0.4 for fibres covered by [ITU-T G.653]) should be used. Light transmitted by the aperture is collected and focused onto the detector.

NOTE – The numerical apertures (NA) of the collecting optics must be large enough not to affect the measurement results.

6.1.2.2.7. Detector (as in clause 6.1.1.2.7)

6.1.2.2.8. Amplifier (as in clause 6.1.1.2.8)

6.1.2.2.9. Data acquisition (as in clause 6.1.1.2.9)

6.1.2.3. Measurement procedure

The launch end of the fibre shall be aligned with the launch beam, and the output end of the fibre shall be aligned to the appropriate output device.

The following procedure shall be followed: the power transmitted by each aperture, P(x), is measured, and the complementary aperture transmission function, a(x), is found as:

$$a(x) = 1 - \frac{P(x)}{P_{\max}} \qquad (6\text{-}2)$$

where $P_{\max}$ is the power transmitted by the largest aperture and x is the aperture radius. The mode field diameter is computed from Equation (6-1).

6.1.2.4. Presentation of the results

The following details shall be presented:

a) test set-up arrangement, dynamic range of the measurement system, processing algorithms, and a description of the aperture assembly used (including the NA);

b) launching conditions;

c) wavelength and spectral line-width FWHM of the source;

d) fibre identification and length;

e) type of cladding mode stripper;

f) description of high-order modes filter;

g) type and dimensions of the detector;

h) temperature of the sample and environmental conditions (when necessary);

i) indication of the accuracy and repeatability;

j) mode field diameter.

6.1.3. Second alternative test method: The near-field scan

6.1.3.1. General

The mode field diameter is determined from the near-field intensity distribution $f^2(r)$ (r being the radial coordinate):

$$2w = 2\left[2\frac{\int_0^\infty r f^2(r)\,dr}{\int_0^\infty r\left[\frac{df(r)}{dr}\right]^2 dr}\right]^{\frac{1}{2}} \qquad (6\text{-}3)$$

The mathematical equivalence of equations Equation (3-2) and Equation (6-3) is valid in the approximation of small angles θ. Under this approximation, the near-field $f(r)$ and the far-field F(θ) form a Hankel pair. By means of the Hankel transform, it is possible to pass from Equation (3-2) to Equation (6-3) and vice versa.

6.1.3.2. Test apparatus

6.1.3.2.1. Light source (as in clause 6.1.1.2.1)

6.1.3.2.2. Modulation (as in clause 6.1.1.2.2)

6.1.3.2.3. Launching conditions (as in clause 6.1.1.2.3)

6.1.3.2.4. Cladding mode stripper (as in clause 6.1.1.2.4)

6.1.3.2.5. Specimen (as in clause 6.1.1.2.5)

6.1.3.2.6. Scan apparatus

Magnifying optics (e.g., a microscope objective) shall be employed to enlarge and focus an image of the fibre near field onto the plane of a scanning detector (for example, a scanning photodetector with a pinhole aperture or a scanning pig-tailed photodetector). The numerical aperture and magnification shall be selected to be compatible with the desired spatial resolution. For calibration, the magnification of the optics should have been measured by scanning the length of a specimen whose dimensions are independently known with sufficient accuracy.

6.1.3.2.7. Detector (as in clause 6.1.1.2.7)

6.1.3.2.8. Amplifier (as in clause 6.1.1.2.8)

6.1.3.2.9. Data acquisition (as in clause 6.1.1.2.9)

6.1.3.3. Measurement procedure

The launch end of the fibre shall be aligned with the launch beam, and the output end of the fibre shall be aligned to the appropriate output device.

The following procedure shall be followed: the near field of the fibre is enlarged by the magnifying optics and focused onto the plane of the detector. The focusing shall be performed with maximum accuracy in order to reduce dimensional errors due to the scanning of a defocused image. The near-field intensity distribution, $f^2(r)$, is scanned and the mode field diameter is calculated from Equation (6-3). Alternatively, the near-field intensity distribution $f^2(r)$ may be transformed into the far-field domain using a Hankel transform and the resulting transformed far-field $F^2(\theta)$ may be used to compute the mode field diameter from Equation (3-2).

NOTE – Discriminate between the radial coordinate r in the fibre end face and the radial coordinate Mr of the scanning detector in the image plane, where M is the magnification.

6.1.3.4. Presentation of the results

The following details shall be presented:

a) test set-up arrangement, dynamic range of the measurement system, processing algorithms, and a description of the imaging and scanning devices used;
b) launching conditions;
c) wavelength and spectral line-width FWHM of the source;
d) fibre identification and length;
e) type of cladding mode stripper;
f) description of high-order modes filter;
g) magnification of the apparatus;
h) type and dimensions of the detector;
i) temperature of the sample and environmental conditions (when necessary);
j) indication of the accuracy and repeatability;
k) mode field diameter.

6.1.4. Third alternative test method: Bidirectional backscatter difference

6.1.4.1. General

The mode field diameter is determined from the difference in bidirectional backscatter across a splice with a dead-zone fibre with a known mode field diameter:

$$w_s = w_d 10^{\frac{g(L_d - L_g)+f}{20}} \quad (6\text{-}4)$$

where::

w_d	is the mode field diameter of the dead-zone fibre
w_s	is the mode field diameter of the specimen fibre
L_d	is the change in backscatter (dB) across the splice when measuring from the dead-zone fibre
L_s	is the change in backscatter (dB) across the splice when measuring from the specimen fibre
g	is a wavelength and fibre design dependent adjustment factor
f	is a wavelength and fibre design dependent adjustment factor

6.1.4.2. Test apparatus

These are as in clause 6.4.2.2, with the following additional requirements:

Figure 2 shows a schematic diagram of an apparatus that uses an optical switch. The use of such apparatus is optional.

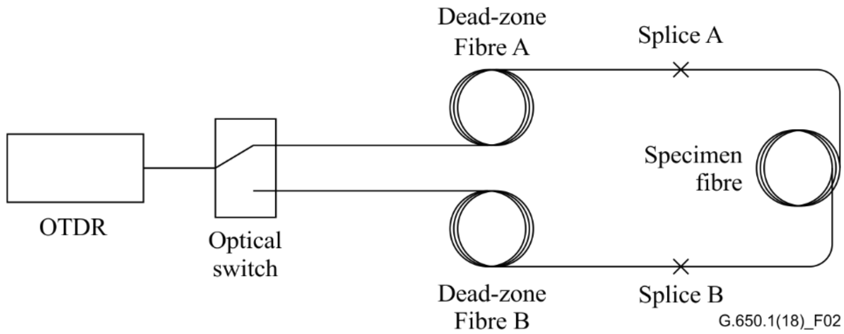


Figure 2 — Optional apparatus for bidirectional backscatter

The optical time domain reflectometer source wavelength shall be known to be within 2 nm. A shift of 2 nm will introduce error of about 0.02 µm for measurements at 1310 nm to 1550 nm.

A dead-zone fibre shall be long enough to prevent the dead-zone region from including the splice or butt-joint with the specimen fibre. The MFD of the dead-zone fibre shall be measured for each wavelength for which measurements are needed with either the RTM or the first or second alternative methods. The dead-zone fibre is typically the same design as the fibre under test.

The splice or butt-joint shall be sufficiently stable over the time the measurement is completed so that the results are not affected. Index matching fluid is recommended when a butt-joint is used in order to minimize reflections.

6.1.4.3. Measurement procedure

This procedure is in two parts: The first is the procedure for a given fibre and wavelength once the adjustment factors, g and f are known. The second is the procedure for qualifying a given fibre type and design at a given wavelength. The qualification procedure includes the accurate calculation of the adjustment factors, g and f, that allow correction for OTDR wavelength off nominal. Where g and f are unknown and accurate determination is impractical, nominal values of 1 and 0, respectively, may be assumed.

6.1.4.3.1. Measurement of a fibre at a given wavelength

a) Align the fibre so that light is launched from the dead-zone fibre A into the specimen fibre. (From the OTDR across splice A into the specimen fibre as shown in Figure 2).

b) Measure the change in backscatter across the splice (splice A as shown in Figure 2), avoiding any reflection, and record the value as L_d.

c) Align the fibre so that light is launched from the specimen fibre into the dead-zone fibre A. (From the OTDR, across splice B into the specimen fibre, then across splice A in Figure 2).

d) Measure the change in backscatter across the splice (splice A as shown in Figure 2), avoiding any reflection, and record the value as L_s.

e) Calculate the mode field diameter according to Equation (6-4).

6.1.4.3.2. Qualification for a fibre type, design and wavelength

a) Select a sample of fibres of the type and design to be measured, for which the mode field diameter, w_s, has been measured at the desired wavelength using either the reference test method or the first or second alternative methods, so that the range of mode field diameter values for the fibre type and design are represented in the sample.

b) Complete procedures a) to d) of clause 6.1.4.3.1 to determine the changes in backscatter across the splice L_d and L_s.

c) Compute $20\log_{10}(w_s / w_d)$ for each fibre and perform a linear regression of it versus $(L_d - L_s)$ to determine g (slope) and f (intercept).

d) Select a second sample of fibres, independent from the first set to determine g and f, for which the mode field diameter has also been measured at the desired wavelength using either the reference test method or the first or second alternative methods.

e) Complete the procedure in clause 6.1.4.3.1, using the values of g and f determined in c) to determine the mode field diameter, w_s. Find the difference to the value measured with the reference test method or the first or second alternative methods.

f) Calculate the average difference (bias), and the standard deviation of differences (σ_d) to determine if equivalence has been demonstrated.

g) An acceptable measure of equivalence may be obtained by calculating the equivalence level, B, where B = |bias| + 2 σ_d/sqrt(n), with n being the sample size. A typical upper limit on B is 0.1 µm.

h) If B exceeds the upper limit, adjustments to the procedure such as improving the splice or butt-joint are recommended.

6.1.4.4. Presentation of results

For each fibre measured the following details shall be presented:

a) nominal wavelength;
b) mode field diameter value;
c) fibre identification.

Information to be available:

a) description of the apparatus;
b) qualification data for each fibre type, design and wavelength;
c) indication of accuracy and repeatability.

6.2. Test methods for the cladding diameter, core concentricity error and cladding non-circularity

6.2.1. Reference test method: The near-field image technique

6.2.1.1. General

The glass geometry parameters are determined from the near-field intensity distribution, according to the definitions given in clause 3.3.3, clause 3.3.5 and clause 3.3.8.

6.2.1.2. Test apparatus

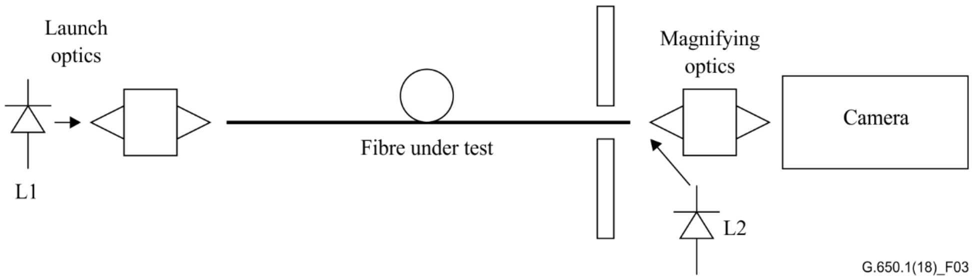


Figure 3 — A scheme for the test apparatus

6.2.1.2.1. Light sources

A light source, L1, for illuminating the core shall be chosen, adjustable in intensity and stable in position, over a period of time which is sufficiently long to complete the measurement procedure. Wavelengths above and/or below the fibre's cut-off wavelength may be used. A second light source, L2, with similar characteristics, shall be used to illuminate the cladding.

6.2.1.2.2. Launching conditions

The launch optics shall be arranged so that the light source uniformly overfills the fibre angularly and spatially. At the output end, the cladding shall be illuminated uniformly.

NOTE – The launching conditions from source L1 shall be such so as to determine a circularly symmetric spatial field distribution at the output of the fibre.

6.2.1.2.3. Cladding mode stripper

Cladding mode light shall be stripped from the specimen near the input end. When the fibre under test has a primary coating with a refractive index higher than that of the glass, this coating acts as a cladding mode stripper.

6.2.1.2.4. Specimen

The specimen shall be a short length of the optical fibre to be measured. The fibre ends shall be clean, smooth and perpendicular to the fibre axis.

6.2.1.2.5. Magnifying optics

The magnifying optics shall consist of an optical system (e.g., a microscope objective) which magnifies the specimen output near field, focusing it onto the plane of the detector. The numerical aperture and hence the resolving power of the optics shall be compatible with the measuring accuracy required, and not lower than 0.3. The magnification shall be selected to be compatible with the desired resolution, and shall be recorded.

6.2.1.2.6. Detector

CCD video cameras, scanning vidicons, or other pattern/intensity recognition devices shall be used to detect the magnified output near-field image and transmit it to a video monitor. The video digitizer performs the digitization of the image for further computer analysis. The video system shall be sufficiently linear so that, after calibration, the measurement uncertainty is not greater than required.

6.2.1.2.7. Video image monitor

A video image monitor shall be used to display the detected image. The screen on the monitor typically shows a pattern, such as cross-hairs, to assist the operator in centring the image of the specimen. Computer-controlled alignment and/or focusing may be used.

6.2.1.2.8. Data system

The measurement, data acquisitions and calculations are performed using a computer. A printer provides a hard copy of the information and measurement results.

6.2.1.3. Measurement procedure

6.2.1.3.1. Calibration

Calibration shall be according to the procedures given in [IEC 61745].

6.2.1.3.2. Measurement

The prepared specimen shall be aligned at the input end to achieve the launch condition specified. The near-field image of the output end shall be focused and centred in the monitor. The intensity of the core image illumination at the input end and the intensity of the cladding image illumination at the output end shall be adjusted according to an established, internal standard for the particular test equipment.

The digitized video image of the output face shall be recorded and the points representing both the cladding image edge and the core image edge shall be determined and recorded in edge tables. The decision levels of the boundaries in the near-field image are the following:

Core image boundary: This level shall be chosen from 5% to 50% of the maximum near-field intensity.

Cladding image boundary: Different methods for determining the cladding boundary can be used, depending on the illumination method. The method used in practice shall be the same as that used in calibration.

6.2.1.3.3. Calculations

The raw data of the core and cladding edge are fitted to smooth, mathematically closed forms to determine best estimates of the actual edges. These smooth mathematically closed forms are then fitted to a circle in order to determine the geometrical characteristics, including the first order deviations from the ideal circular shape of each respective edge boundary. These values and the mathematical edge representation are used to determine the parameters as follows:

– X_{co}, Y_{co} (µm) fitted core centre;
– R_{cl} (µm) fitted cladding radius;
– X_{cl}, Y_{cl} (µm) fitted cladding centre;
– R_{mincl} (µm) minimum distance of the cladding edge to centre;
– R_{maxcl} (µm) maximum distance of the cladding edge to centre;
– cladding diameter (µm) = $2R_{cl}$;
– cladding non-circularity (%) = $100(R_{maxcl} - R_{mincl})/R_{cl}$;
– core concentricity error (µm) = $[(X_{cl} - X_{co})^2 + (Y_{cl} - Y_{co})^2]^{1/2}$.

The smooth mathematically closed forms used to represent the edges are required to allow a variation of curvature that is greater than or equal to that found in an ellipse. For non-elliptical forms, the data can be converted to polar coordinates about a roughly estimated centre before fitting the radius versus angular position.

Active filtering, or removal of raw data points that represent cleave damage from those that are fitted to the mathematical form, is allowed. The choice of the curve, the equipment, the cleave method and the filtration algorithm are interactive in their contribution to the quality of the cladding measurement results.

6.2.1.4. Presentation of the results

For each measurement the following details shall be presented:

a) fibre identification;
b) the parameters: cladding diameter, cladding non-circularity and core concentricity error.

Information to be available:

a) test set-up arrangement;
b) launching conditions;
c) spectral characteristics;
d) magnification factor;
e) type and dimensions of the detector;
f) indication of accuracy and repeatability, including calibration data.

6.2.2. First alternative test method: The refracted near-field technique

6.2.2.1. General

The refracted near-field measurement gives directly the refractive index distribution across the entire fibre (core and cladding). The geometrical characteristics of the fibre can be obtained from the refractive index distribution using suitable algorithms.

6.2.2.2. Test apparatus

A schematic diagram of the measurement method is shown in Figure 4. The technique involves the scanning of a focused spot of light across the end of the fibre. The launch optics are arranged to overfill the numerical aperture of the fibre. The fibre end is immersed in a fluid of slightly higher index than the cladding. Part of the light is guided down the fibre and the rest appears as a hollow cone outside the fibre. A disc is placed on the axis of the core to ensure that only refracted light reaches the detector.

The optical resolution, and hence the ability to resolve details in the fibre geometry, depends on the size of the focused spot of light. This depends both on the numerical aperture of the focusing lens and on the size of the disc. However, the position of sharp features can be resolved to much better accuracy than this, dependent on step size for stepper motor systems, or position monitoring accuracy of analogue drives.

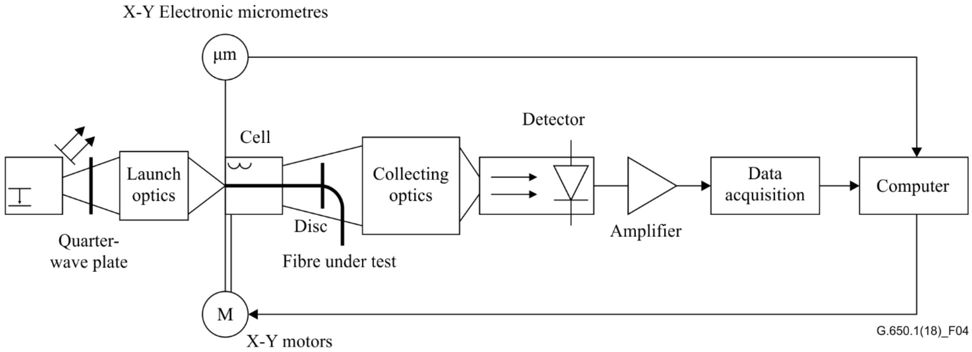


Figure 4 — Typical arrangement of the refracted near-field test set-up

6.2.2.2.1. Source

A stable laser giving about 1 mW of power in the TEM_{00} mode is required, such as a HeNe laser.

A quarter-wave plate is introduced to change the beam from linear to circular polarization because the reflectivity of light at an air-glass interface is strongly angle and polarization-dependent.

6.2.2.2.2. Launching conditions

The launch optics, which are arranged to overfill the numerical aperture of the fibre, bring a beam of light to a focus on the flat end of the fibre. The optical axis of the beam of light should be within 1° of the axis of the fibre. The resolution of the equipment is determined by the size of the focused spot, which should be as small as possible in order to maximize the resolution, e.g., less than 1.0 µm. The equipment enables the focused spot to be scanned across the fibre cross section.

6.2.2.2.3. Cell

The cell will contain a fluid with a refractive index slightly higher than that of the fibre cladding. The position of the cell will be controlled by X-Y motors driven by the computer and detected by X-Y micrometres.

6.2.2.2.4. Detection

The refracted light is collected by suitable collecting optics and brought to the detector in any convenient manner provided that all the refracted light is collected. By calculation, the required size of disc and its position along the central axis can be determined.

6.2.2.2.5. Data acquisition

The measured intensity distribution can be recorded, processed and presented in a suitable form, according to the scanning technique and to the specification requirements. A computer will be used to drive the X-Y motors, to record the X-Y position of the cell and the corresponding power levels, and to process the measured data.

6.2.2.3. Procedure

Refer to the schematic diagram of the test apparatus (Figure 4).

6.2.2.3.1. Preparation of fibre under test

A length of fibre less than 2 m is required.

The primary fibre coating shall be removed from the section of fibre immersed in the fluid cell.

The fibre ends shall be clean, smooth and perpendicular to the fibre axis.

6.2.2.3.2. Equipment calibration

The equipment is calibrated with the fibre removed from the fluid cell. During the measurement, the angle of the cone of light varies according to the refractive index seen at the entry point to the fibre (hence the change of power passing the disc). With the fibre removed and the fluid index and cell thickness known, this change in angle can be simulated by translating the disc along the optic axis. By moving the disc to a number of predetermined positions, one can scale the profile in terms of relative index. Absolute index can only be found if the cladding or fluid index is known accurately at the measurement wavelength and temperature.

More convenient calibration procedures can be performed by means of a thin rod of known constant refractive index or by means of a multimode-multistep fibre, where the various refractive index values are known with great accuracy. This latter technique can also be useful in checking the linearity of the apparatus. In this respect, it may also be useful to control the fluid temperature in the fluid cell.

6.2.2.3.3. Raster scan

The launch end of the fibre to be measured is immersed in the fluid cell and the laser beam is simultaneously centred and focused on the fibre end face.

The disc is centred on the output cone. Refracted modes passing the disc are collected and focused onto the detector.

The focused laser spot is scanned across the fibre end cross section and a two-dimensional distribution of fibre refractive index is directly obtained. From this distribution, the geometrical characteristics will be calculated.

6.2.2.3.4. Geometrical characteristics

Once the raster scan of refractive index is performed, the core contour is obtained taking the points at the core-cladding interface of refractive index coinciding with the mean value between the averaged refractive indices of core and cladding respectively. The cladding contour is determined in a similar way but at the cladding-index matching fluid interface. Geometry analyses consistent with the terms in clause 3 will be performed starting from the core and cladding contours data. An index profile measurement actually yields the core concentricity error.

6.2.2.4. Presentation of the results

The following details shall be presented:
a) test set-up arrangement and indication of the scanning technique used;
b) fibre identification;
c) cladding diameter;
d) core concentricity error;
e) cladding non-circularity;
f) core diameter (if required);
g) raster scan across the entire fibre (if required);
h) indication of accuracy and repeatability;
i) temperature of the sample and environmental conditions (if necessary).

6.2.3. Second alternative test method: The side-view technique

6.2.3.1. General

The side-view method is applied to single-mode fibres to determine geometrical parameters (core concentricity error, cladding diameter and cladding non-circularity) by measuring the intensity distribution oflight that is refracted inside the fibre.

6.2.3.2. Test apparatus

Aschematic diagram of the test apparatus is shown in Figure 5.

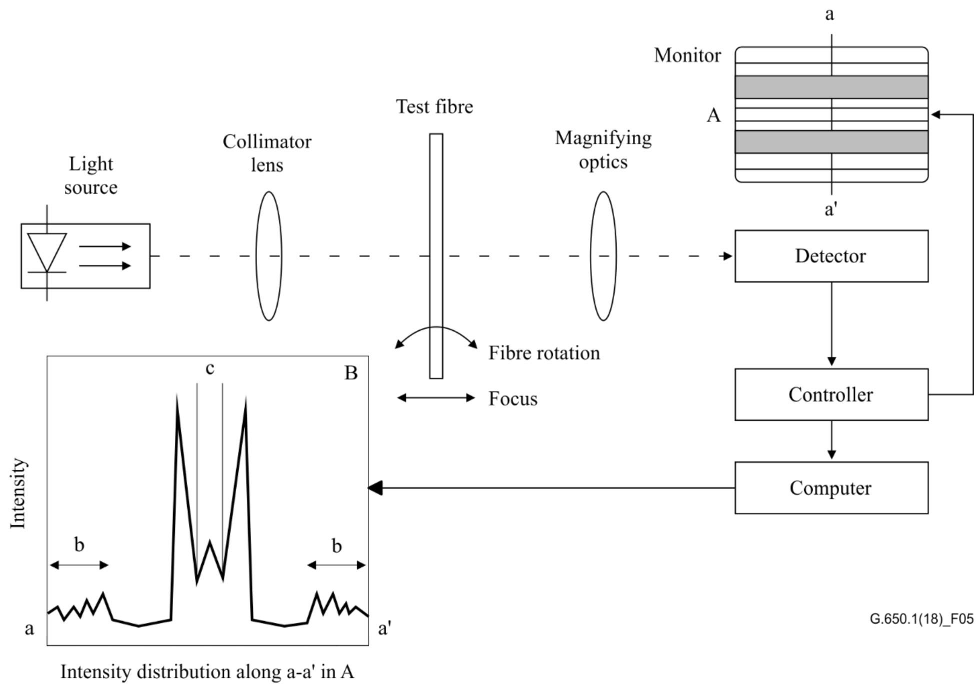


Figure 5 — Schematic diagram of side-view measurement system

6.2.3.2.1. Light source

The emitted light shall be collimated, adjustable in intensity and stable in position, intensity and wavelength over a time period sufficiently long to complete the measuring procedure. A stable and high intensity light source such as a light emitting diode (LED) may be used.

6.2.3.2.2. Specimen

The specimen to be measured shall be a short length of single-mode fibre. The primary fibre coating shall be removed from the observed section of the fibre. The surface of the fibre shall be kept clean during the measurement.

6.2.3.2.3. Magnifying optics

The magnifying optics shall consist of an optical system (e.g., a microscope objective) which magnifies the intensity distribution of refracted light inside the fibre onto the plane of the scanning detector. The observation plane shall be set at a fixed distance forward from the fibre axis. The magnification shall be selected to be compatible with the desired spatial resolution and shall be recorded.

6.2.3.2.4. Detector

A suitable detector shall be employed to determine the magnified intensity distribution in the observation plane along the line perpendicular to the fibre axis. A vidicon or charge coupled device can be used. The detector must have linear characteristics in the required measuring range. The detector's resolution shall be compatible with the desired spatial resolution.

6.2.3.2.5. Data processing

A computer with appropriate software shall be used for the analysis of the intensity distributions.

6.2.3.3. Measurement procedure

6.2.3.3.1. Equipment calibration

For equipment calibration, the magnification of the magnifying optics shall be measured by scanning the length of a specimen whose dimensions are already known with suitable accuracy. This magnification shall be recorded.

6.2.3.3.2. Measurement

The test fibre is fixed in the sample holder and set in the measuring system. The fibre is adjusted so that its axis is perpendicular to the optical axis of the measuring system.

Intensity distributions in the observation plane along the line perpendicular to the fibre axis (a-a' in A, in Figure 5) are recorded (shown as B) for different viewing directions, by rotating the fibre around its axis, keeping the distance between the fibre axis and the observation plane constant. The cladding diameter and the central position of the fibre are determined by analysing the symmetry of the radial intensity distribution in the magnified image (shown as b in B). The central position of the core is determined by analysing the intensity distribution of converged light (shown as c). The distance between the central position of the fibre and that of the core corresponds to the nominal observed value of core concentricity error.

As shown in Figure 6, fitting the sinusoidal function to the experimentally obtained values of the mode field concentricity error (see clause 3.3.7, Note 2) plotted as a function of the rotation angle, the actual core concentricity error is calculated as the product of the maximum amplitude of the sinusoidal function and magnification factor with respect to the lens effect due to the cylindrical structure of the fibre. The cladding diameter is evaluated as an averaged value of measured fibre diameters at each rotation angle, resulting in values for maximum and minimum diameters to determine the value of cladding non-circularity according to the definition.

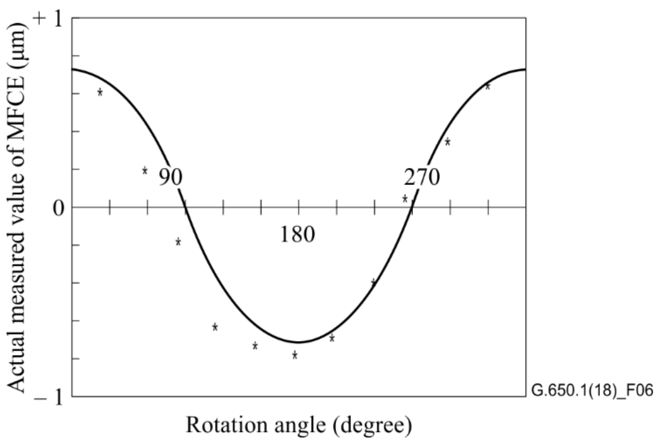


Figure 6 — Measured value of the mode field concentricity error as a function of rotation angle

6.2.3.4. Presentation of the results

The following details shall be presented:

a) test arrangement;
b) fibre identification;
c) spectral characteristics of the source;
d) indication of repeatability and accuracy;
e) plot of nominal core concentricity error versus rotation angle;
f) core concentricity error, cladding diameter and cladding non-circularity;
g) temperature of the sample and environmental conditions (if necessary).

6.2.4. Third alternative test method: The transmitted near-field technique

6.2.4.1. General

The geometrical parameters are determined from the near-field intensity distribution according to the definitions given in clause 3.3.3, clause 3.3.5 and clause 3.3.8.

Since mode field concentricity is a good approximation of core concentricity, this method can be used to evaluate core concentricity error.

6.2.4.2. Test apparatus

A schematic diagram of the test apparatus is shown in Figure 7.

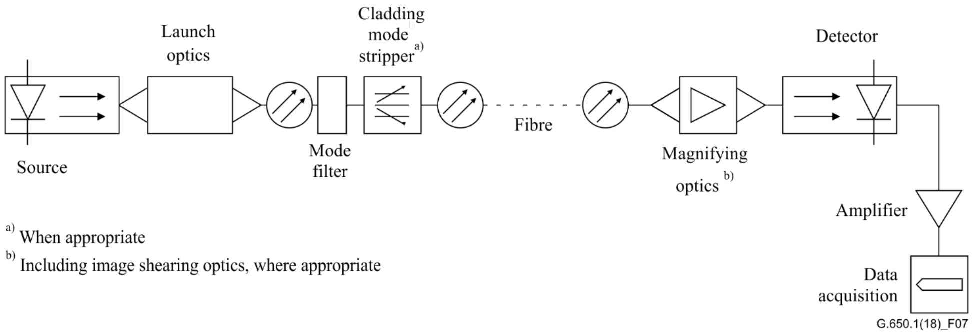


Figure 7 — Typical arrangement of the transmitted near-field set-up

6.2.4.2.1. Light source

A nominal 1310 nm (for fibres covered by [ITU-T G.652]) or 1550 nm (for fibres covered by [ITU-T G.653] and [ITU-T G.654]) light source for illuminating the core shall be used. The light source shall be adjustable in intensity and stable in position, intensity and wavelength over a time period sufficiently long to complete the measurement procedure. The spectral characteristics of this source should be chosen to preclude multimode operation. A second light source with similar characteristics can be used, if necessary, for illuminating the cladding. The spectral characteristics of the second light source must not cause defocusing of the image.

6.2.4.2.2. Launching conditions

The launch optics, which will be arranged to overfill the fibre, will bring a beam of light to a focus on the flat input end of the fibre.

6.2.4.2.3. Mode filter

In the measurement, it is necessary to assure single-mode operation at the measurement wavelength. In these cases, it may be necessary to introduce a bend in order to remove the LP_{11} mode.

6.2.4.2.4. Cladding mode stripper

A suitable cladding mode stripper shall be used to remove the optical power propagating in the cladding. Whenmeasuring the geometrical characteristics of the cladding only, the cladding mode stripper shall not be present.

6.2.4.2.5. Specimen

The specimen shall be a short length of the optical fibre to be measured. The fibre ends shall be clean, smooth and perpendicular to the fibre axis.

6.2.4.2.6. Magnifying optics

The magnifying optics shall consist of an optical system (e.g., a microscope objective) which magnifies the specimen output near field, focusing it onto the plane of the scanning detector. The numerical aperture, and hence the resolving power ofthe optics, shall be compatible with the measuring accuracy required, and not lower than 0.3. The magnification shall be selected to be compatible with the desired spatial resolution, and shall be recorded.

6.2.4.2.7. Detector

A suitable detector shall be employed which provides the point-to-point intensity of the transmitted near-field pattern(s). For example, any of the following techniques can be used:

a) scanning photodetector with pinhole aperture;
b) scanning mirror with fixed pinhole aperture and photodetector;
c) scanning vidicon, charge coupled devices or other pattern/intensity recognition devices.

The detector shall be linear (or shall be linearized) in behaviour over the range of intensities encountered.

6.2.4.2.8. Amplifier

An amplifier may be employed in order to increase the signal level. The bandwidth of the amplifier shall be chosen according to the type of scanning used. When scanning the output end of the fibre with mechanical or optical systems, it is customary to modulate the optical source. Ifsuch a procedure is adopted, the amplifier should be linked to the source modulation frequency.

6.2.4.2.9. Data acquisition

The measured intensity distribution can be recorded, processed and presented in a suitable form, according to the scanning technique and to the specification requirements.

6.2.4.3. Measurement procedure

6.2.4.3.1. Equipment calibration

For equipment calibration, the magnification of the magnifying optics shall be measured by scanning the image of a specimen whose dimensions are already known with suitable accuracy.

This magnification shall be recorded.

6.2.4.3.2. Measurement

The launch end of the fibre shall be aligned with the launch beam, and the output end of the fibre shall be aligned to the optical axis of the magnifying optics. For transmitted near-field measurement, the focused image(s) of the output end of the fibre shall be scanned by the detector, according to the specification requirements. The focusing shall be performed with maximum accuracy, in order to reduce dimensional errors due to the scanning of a defocused image. The desired geometrical parameters are then calculated according to the definitions.

Algorithms for defining edges and calculating the geometrical parameters are under study.

6.2.4.4. Presentation of the results

The following details shall be presented:

a) test set-up arrangement, with indication of the scanning technique used;
b) launching conditions;
c) spectral characteristics of the source(s);
d) fibre identification and length;
e) type of mode filter (if applicable);
f) magnification of the magnifying optics;
g) type and dimensions of the scanning detector;
h) temperature of the sample and environmental conditions (when necessary);
i) indication of the accuracy and repeatability;

j) resulting dimensional parameters, such as cladding diameters, cladding non-circularities, core concentricity error, etc.

6.3. Test methods for the cut-off wavelength

6.3.1. Reference test method for the fibre cut-off wavelength (λ_c) of the primary coated fibre: The transmitted power technique

6.3.1.1. General

The cut-off wavelength measurement of single-mode fibres is intended to assure effective single-mode operation above a specified wavelength.

The cut-off wavelength measurement shall use the transmitted power technique which measures the variation with wavelength of the transmitted power of a short length of the fibre under test, under defined conditions, compared to a reference transmitted power. There are two possible ways to obtain this reference power:

a) the test fibre with a loop of smaller radius; or

b) a short (1-2 m) length of multimode fibre.

NOTE 1 –

In this version of this Recommendation, the ATM for λc measurement found in the previous versionare incorporatedin an RTM.

NOTE 2 –

The presence of a primary coating on the fibre usually does not affect the cut-off wavelength. However, the presence of a secondary coating may result in a cut-off wavelength that may be significantly shorter than that of the primary coated fibre.

The measurement may be performed on a fibre having a secondary coating if the secondary coating type has been examined and it has been confirmed that it does not significantly affect the cut-off wavelength, provided that the secondary coating is properly applied.

6.3.1.2. Test apparatus

6.3.1.2.1. Light source

A light source with a line width not exceeding 10 nm (FWHM), stable in position, intensity and wavelength over a time period which is sufficient to complete the measurement procedure, and capable of operating over a sufficient wavelength range, shall be used.

6.3.1.2.2. Modulation

It is customary to modulate the light source in order to improve the signal/noise ratio at the receiver. If such a procedure is adopted, the detector should be linked to a signal processing system synchronous with the source modulation frequency. The detecting system should be substantially linear.

6.3.1.2.3. Launching conditions

The launching conditions must be used in such a way as to excite substantially and uniformly both LP_{01} and LP_{11} modes. For example, suitable launching techniques could be:

a) jointing with a multimode fibre; or

b) launching with a suitable large spot-large NA optics.

6.3.1.2.4. Cladding mode stripper

The cladding mode stripper is a device that encourages the conversion of cladding modes to radiation modes; as a result, cladding modes are stripped from the fibre. Care should be taken to avoid affecting the propagation of the LP_{11} mode.

6.3.1.2.5. Optical detector

A suitable detector shall be used so that all of the radiation emerging from the fibre is intercepted. The spectral response should be compatible with the spectral characteristics of the source. The detector must be uniform and have linear sensitivity.

6.3.1.3. Measurement procedure

6.3.1.3.1. Standard test sample

The measurement shall be performed on a 2 m length of fibre. The fibre is inserted into the test apparatus and bent to form a loosely constrained loop. The loop shall complete one full turn of a circle of 140 mm radiusor a full turn (360 degrees) consisting of two arcs (180 degrees each) of 140 mm radius, connected by tangents (split mandrel configuration). The remaining part of the fibre shall be substantially free of external stresses. While some incidental bends of larger radii are permissible, they must not introduce a significant change in the measurement result. The output power $P_1(\lambda)$ shall be recorded versus λ in a sufficiently wide range around the expected cut-off wavelength.

In split mandrel configuration as shown in Figure 8, the lower semicircular mandrel moves to take any slack from the fibre loop without requiring movement of the launch or receive optics or placing the fibre sample under any significant tension.

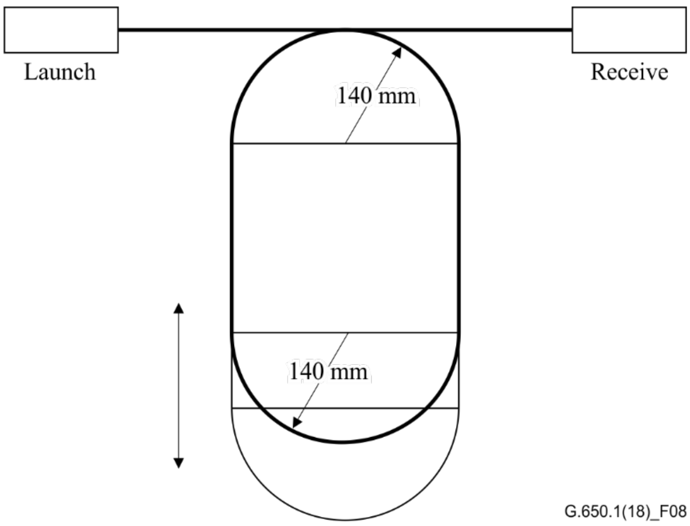


Figure 8 — Fibre deployment: Cut-off wavelength by the split-mandrel technique

6.3.1.3.2. Transmission through the reference sample

Either method a) or b) may be used.

a) Using the test sample, and keeping the launch conditions fixed, an output power $P_2(\lambda)$ is measured over the same wavelength range with at least one loop of sufficiently small radius in the test sample to filter the LP_{11} mode. The exact value of the smaller radius may be determined prior to measurement. It should be small enough to attenuate the second-order mode but not the primary mode, but not too small in order to avoid macrobending effects at higher wavelengths. Aradius between 10 and 30 mm is typical for most ITU-TG.65x fibres. For some [ITU-T G.657] fibres, the radius shall be much smaller, and this measurement procedure may not be adequate for these fibres. See Note 2.

b) With a short (1-2 m) length of multimode fibre, an output power $P_3(\lambda)$ is measured over the same wavelength range.

NOTE 1 – The presence of leaky modes may cause ripple in the transmission spectrum of the multimode reference fibre, affecting the result. To reduce this problem, light-launching conditions may be restricted to fill only 70% of the multimode fibre's core diameter and NA or a suitable mode filter may be used.

NOTE 2 – For some [ITU-T G.657] fibres, because of the bending-loss insensitive nature of these fibres, method a) may not be adequate, it is recommended to use method b) as a reference scan for these fibres.

6.3.1.3.3. Calculations

The spectral attenuation of the test specimen, relative to the reference power is:

$$a(\lambda) = 10\log\frac{P_1(\lambda)}{P_i(\lambda)} \quad (6\text{-}5)$$

where $i = 2$ or 3 for methods a) or b), respectively, in clause 6.3.1.3.2.

Assuming a straight-line representation of the upper wavelength region, the deviation of higher-order modes from the fundamental mode is:

$$\Delta a(\lambda) = a(\lambda) - (A_u + B_u\lambda) \quad (6\text{-}6)$$

A_u and B_u are determined so that $(A_u + B_u\lambda)$ represents the portion of the spectral attenuation curve at wavelengths above the region where the attenuation of higher order modes is accelerated (transition region). For method a), both A_u and B_u may be set to zero. See Figure 9-a and Figure 10-a.

NOTE – In method a) in clause 6.3.1.3.2, the small mode filter fibre loop eliminates all modes except the fundamental one for wavelengths greater than a few tens of nm below the cut-off wavelength λ_c. For wavelengths more than several hundred nm above λ_c, even the fundamental mode may be strongly attenuated by the loop. a(λ) is equal to the logarithmic ratio between the total power emerging from the sample, including the LP_{11} mode power, and the fundamental mode power. When the modes are uniformly excited in accordance with clause 6.3.1.2.3, a(λ) then also yields the LP_{11} mode attenuation A(λ) in dB in the test sample:

$$A(\lambda) = 10\log\left(\frac{P_1(\lambda)}{P_2(\lambda)} - 1\right)/2 \quad (6\text{-}7)$$

6.3.1.3.4. Determination of cut-off wavelength

In the transition region, higher-order mode power is reduced with increasing wavelength. Fibre cut-off wavelength, λ_c, is defined as the wavelength at which the higher-order mode power relative to the fundamental mode power, Δa(λ), has been reduced to 0.1 dB.

Figure 9-b and Figure 10-b illustrate "humps" that sometimes appear near the cut-off wavelength. In the absence of humps (see Figure 9-a and Figure 10-a), accurate determination of λ_c can be achieved without algorithms. Optionally, for precision improvement, fitting algorithms based on the following equations can be used when humps are present. Appendix I contains examples of such algorithms.

$$\gamma(\lambda) = 10\log - \frac{10}{A}\log\frac{10^{\Delta a(\lambda)/10} - 1}{\rho} \quad (6\text{-}8)$$

$$A = 10\log\lfloor\rho/(10^{0.01} - 1)\rfloor \quad (6\text{-}9)$$

Unless otherwise specified,

$$\rho = 2 \quad (6\text{-}10)$$

When the coefficients of:

$$A_t + B_t\lambda = -Y(\lambda) \quad (6\text{-}11)$$

are determined for wavelengths in the transition region, then:

$$\lambda_c = -\frac{A_t}{B_t} \quad (6\text{-}12)$$

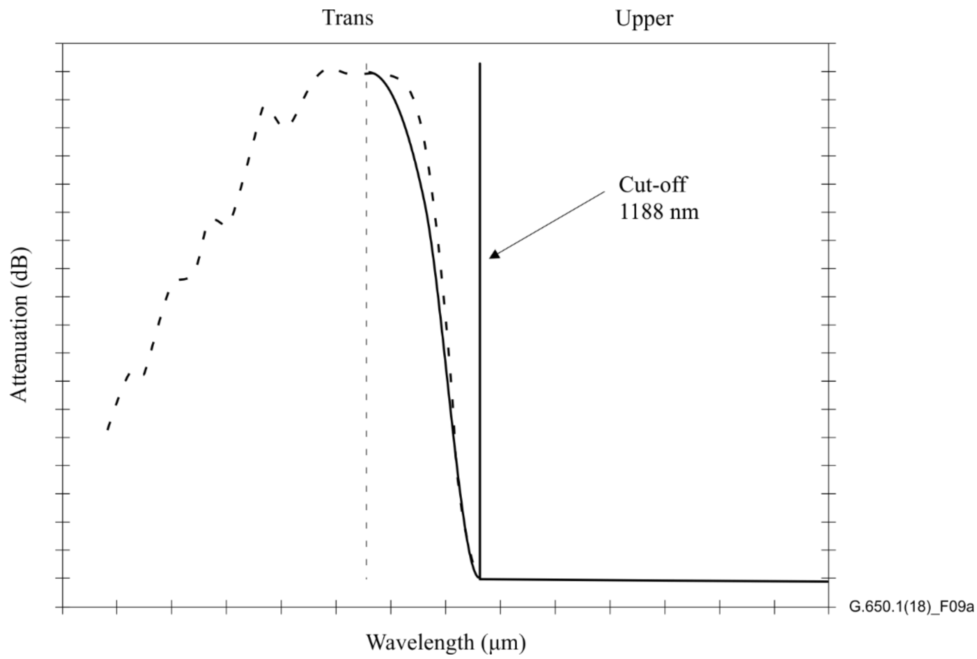


Figure 9-a — Single-mode reference cut-off plot

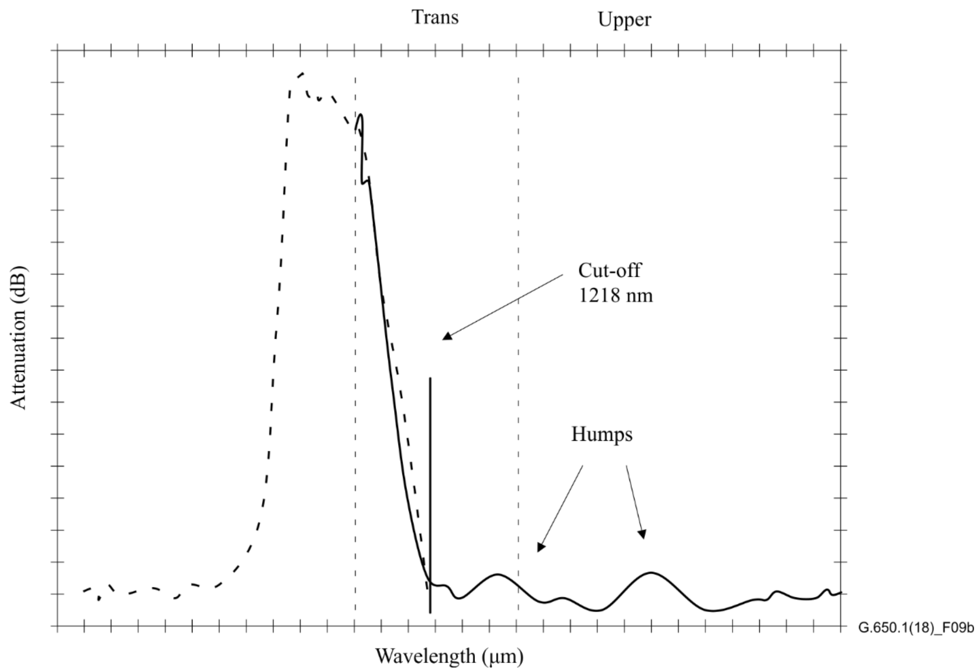


Figure 9-b — Single-mode reference cut-off plot with humps

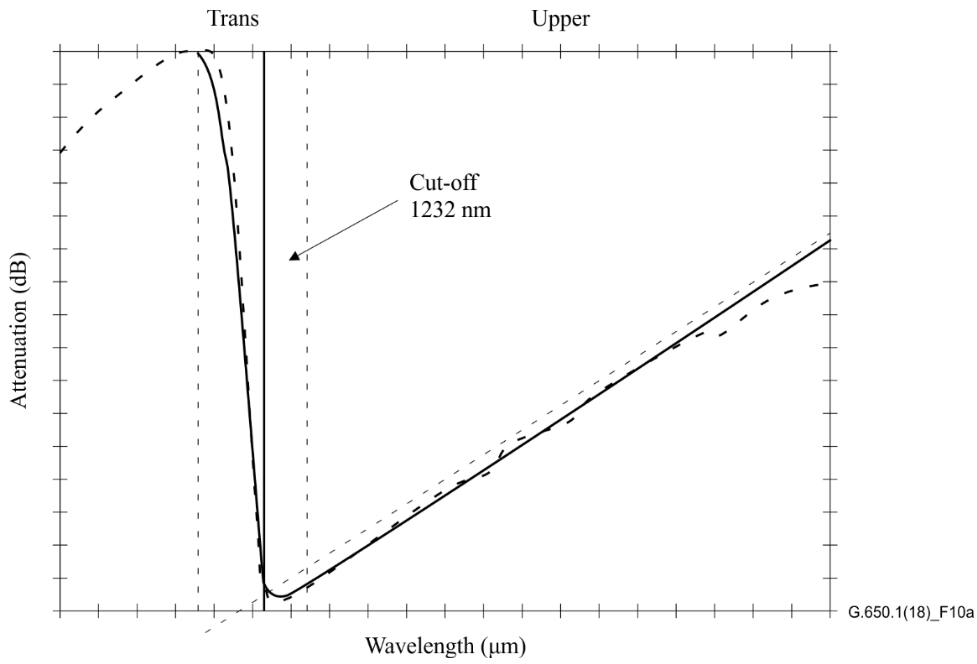


Figure 10-a — Multimode reference cut-off plot

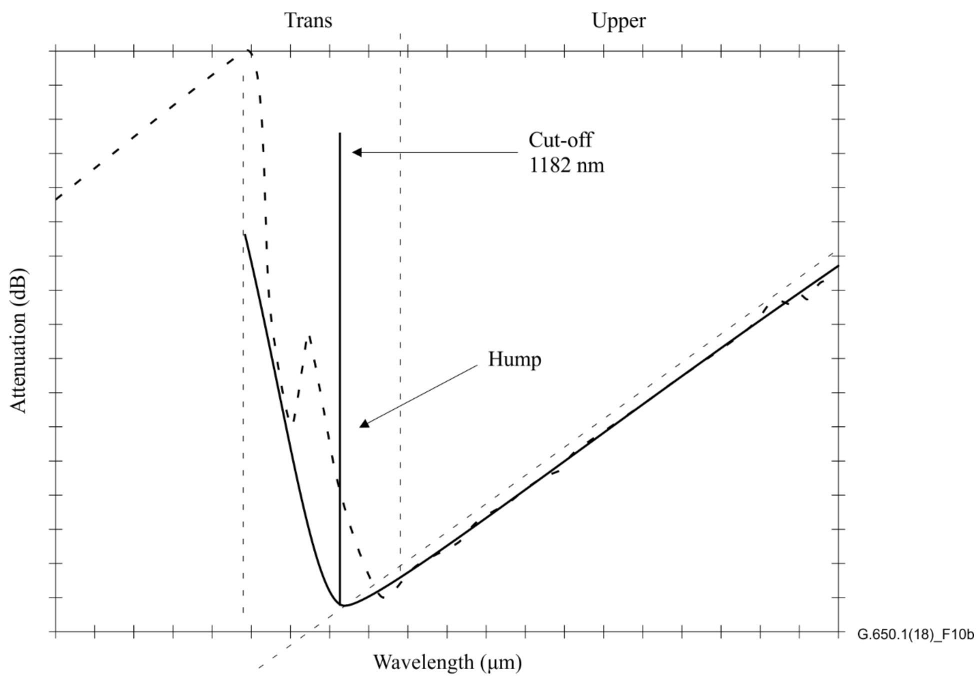


Figure 10-b — Multimode reference cut-off plot with hump

NOTE – According to the definition, the LP_{11} mode attenuation in the test sample is 19.3 dB at the cut-off wavelength.

6.3.1.4. Presentation of the results

The following details shall be presented:

a) test set-up arrangement;
b) launching condition;
c) type of reference sample;
d) temperature of the sample and environmental conditions (if necessary);
e) fibre identification;
f) wavelength range of measurement;
g) fibre cut-off wavelength;

h) plot of a(λ) (if required);
i) interpolation method (if used).

6.3.2. Reference test method for the cable cut-off wavelength (λ_{cc}): The transmitted power technique

6.3.2.1. General

This cut-off wavelength measurement, which is performed on cabled single-mode fibres in a deployment condition which simulates outside plant minimum cable lengths, is intended to assure effective single-mode operation above a specified wavelength.

The transmitted power technique uses the variation with wavelength of the transmitted power of the fibre cable under test, under defined conditions, compared to a reference transmitted power. There are two possible ways to obtain this reference power:
a) the cabled test fibre with a loop of smaller radius;
b) a short (1-2 m) length of multimode fibre.

NOTE – In this version of this Recommendation, the ATM for λ_{cc} measurement found in the previous version is incorporated in an RTM.

6.3.2.2. Test apparatus

6.3.2.2.1. Light source (as in clause 6.3.1.2.1)

6.3.2.2.2. Modulation (as in clause 6.3.1.2.2)

6.3.2.2.3. Launching conditions (as in clause 6.3.1.2.3)

6.3.2.2.4. Cladding mode stripper (as in clause 6.3.1.2.4)

6.3.2.2.5. Optical detector (as in clause 6.3.1.2.5)

6.3.2.3. Measurement procedure

6.3.2.3.1. Standard test sample

The measurement shall be performed on a length of single-mode fibre in a cable. A cable length of 22 m shall be prepared by exposing 1 m uncabled fibre length at each end, and the resulting 20 m cabled portion shall be laid without any small bends which could affect the measurement value. To simulate the effects of a splice organizer, one loop of X = 40 mm radius shall be applied to each uncabled fibre length (see Figure 11). The uncabled fibre is deployed with secondary coating (if present) intact. While some incidental bends of larger radii are permissible in the fibre or cable, they must not introduce a significant change in the measurements. The output power $P_1(\lambda)$ shall be recorded versus λ in a sufficiently wide range around the expected cut-off wavelength.

Alternatively, uncabledsingle-mode fibre in a deployment condition can be used as a test sample which assures that the results for λ_{cc} are in agreement with those achieved in measurements conducted on cabled fibres.

A fibre length of 22 m is inserted into the test apparatus; the inner 20 m are bent to form loosely constrained loops of a radius $r \geq 140$ mm. One loop of X = 40 mm radius shall be applied to each fibre end (see Figure 12).

Though the relationship between λ_{cc} values measured with cabled and uncabled fibre samples depends on the specific cable design, λ_{cc} measured with an uncabled fibre sample is generally higher than that measured with a cabled fibre sample.

NOTE 1 – The loops are intended to simulate deployment conditions.

NOTE 2 – Two loops of X = 40 mm radius at one end can be substituted for one loop at each end.

NOTE 3 – λ_{cc} measurement using a cabled or uncabled test sample found in clause 6.3.2 is described in Annex B or Annex A in [IEC 60793-1-44], respectively.

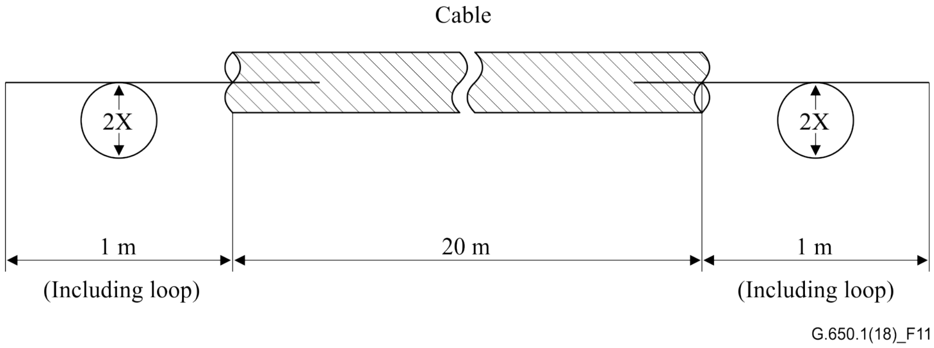


Figure 11 — Deployment condition for measurement of λ_{cc} on cabled fibre

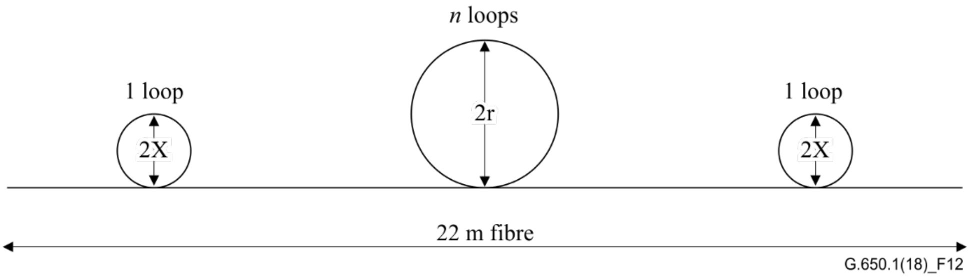


Figure 12 — Deployment condition for measurement of λ_{cc} on uncabled fibres

6.3.2.3.2. Transmission through the reference sample (as in clause 6.3.1.3.2)

6.3.2.3.3. Calculations

The logarithmic ratio between the transmitted powers $P_1(\lambda)$ and $P_i(\lambda)$ is calculated as:

$$R(\lambda) = 10\log\frac{P_1(\lambda)}{P_i(\lambda)} \tag{6-13}$$

where i = 2 or 3 for methods a) or b) in clause 6.3.1.3.2, respectively.

6.3.2.3.4. Determination of cabled fibre cut-off wavelength

The calculations and method of determining cable cut-off wavelength, λ_{cc}, are the same as for fibre cut-off wavelength. See clauses clause 6.3.1.3.3 and clause 6.3.1.3.4.

6.3.2.4. Presentation of the results

The following details shall be presented:

a) test set-up arrangement;
b) launching condition;
c) type of reference sample;
d) temperature of the sample and environmental conditions (if necessary);
e) fibre and cable identification;
f) wavelength range of measurement;
g) cabled fibre cut-off wavelength;
h) plot of $R(\lambda)$ (if required);
i) value of fibre loop radius r (only for uncabled test sample).

6.4. Test methods for attenuation

The attenuation tests are intended to provide a means whereby a certain attenuation value may be assigned to a fibre length so that individual attenuation values may be added together to determine the total attenuation of a concatenated length.

6.4.1. Reference test method: The cut-back technique

6.4.1.1. General

The cut-back technique is a direct application of the definition in which the power levels P_1 and P_2 are measured at two points of the fibre without a change of input conditions. P_2 is the power emerging from the far end of the fibre, and P_1 is the power emerging from a point near the input after cutting the fibre.

6.4.1.2. Test apparatus

Measurements may be made at one or more spot wavelengths, or alternatively, a spectral response may be required over a range of wavelengths. Diagrams of suitable test equipment, to obtain one loss or the loss spectrum measurements respectively, are shown as examples in Figure 13.

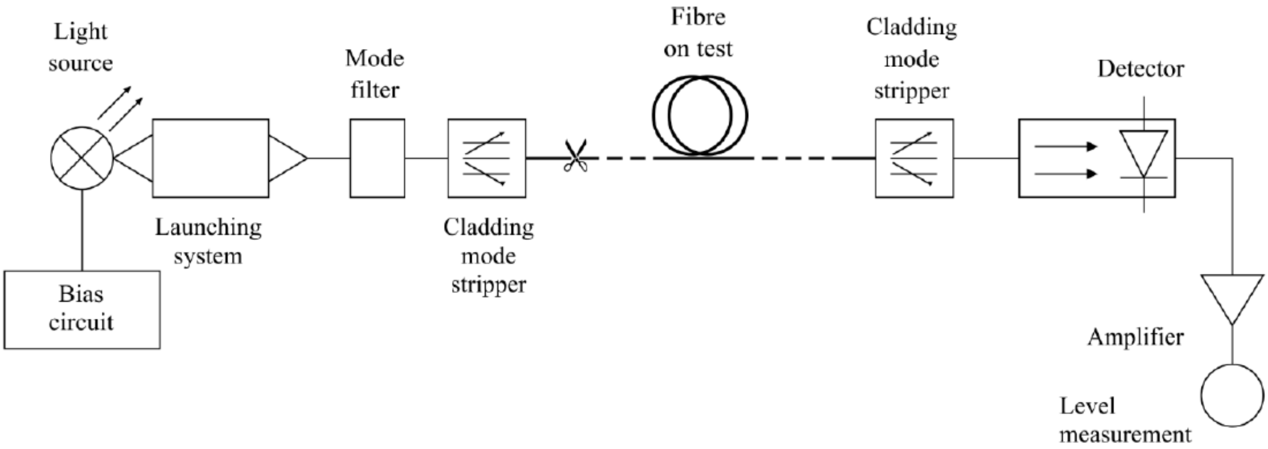


Figure 13-a — Arrangement of test equipment to make one loss measurement

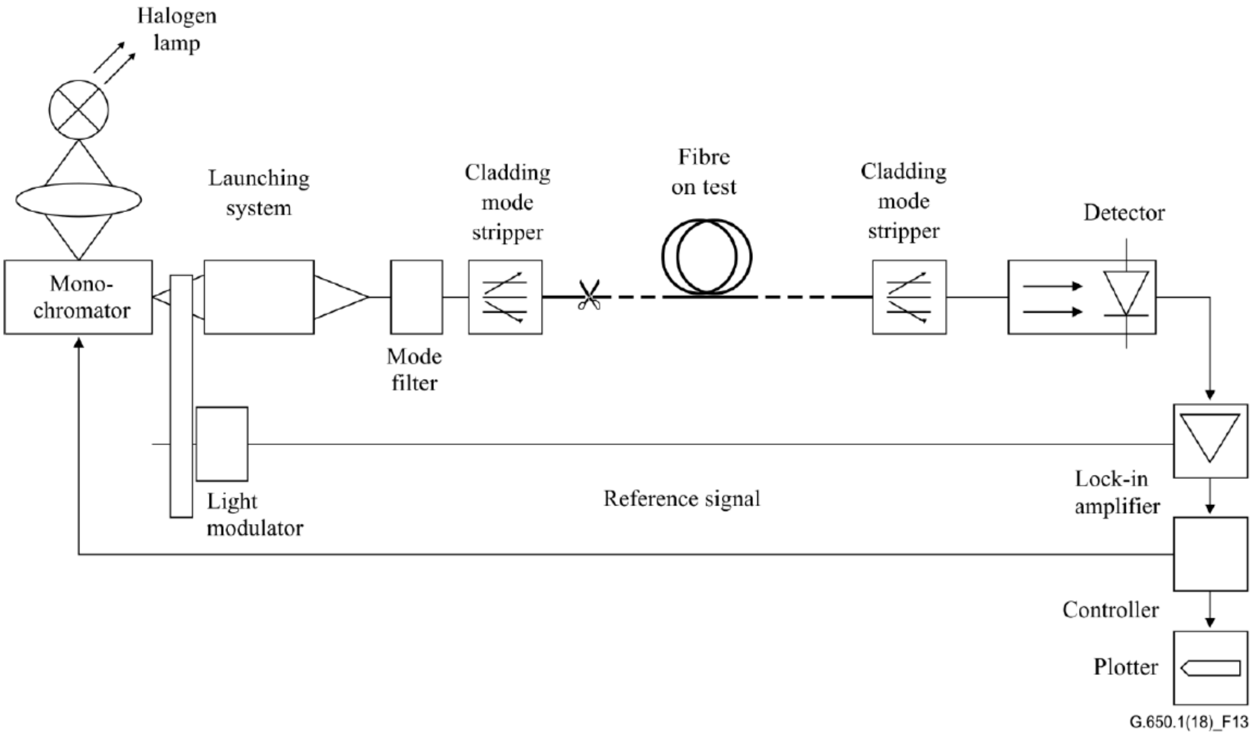


Figure 13-b — Arrangement of test equipment used to obtain the loss spectrum measurement

Figure 13 — The cut-back technique

6.4.1.2.1. Optical source

A suitable radiation source shall be used as a lamp, laser or light emitting diode. The choice of source depends upon the type of measurement. The source must be stable in position, intensity and wavelength over a time period sufficiently long to complete the measurement procedure. The spectral line width (FWHM) shall be specified so that the line width is narrow compared with any features of the fibre spectral attenuation.

6.4.1.2.2. Modulation

It is customary to modulate the light source in order to improve the signal/noise ratio at the receiver. If such a procedure is adopted, the detector should be linked to a signal processing system synchronous with the source modulation frequency. The detecting system should be substantially linear in sensitivity.

6.4.1.2.3. Launching conditions

The launching conditions used must be sufficient to excite the fundamental mode. For example, suitable launching techniques could be:

a) jointing with a fibre;

b) launching with a suitable system of optics.

6.4.1.2.4. Mode filter

Care must be taken that higher order modes do not propagate through the cut-back length. In these cases, it may be necessary to introduce a bend in order to remove the higher modes. For example, a one-turn bend with a radius of 30 mm on the fibre is generally sufficient for most ITU-T G.65x fibres. For some [ITU-T G.657] fibres, smaller radius, multiple bends or longer sample length can be applied to remove high-order propagating modes.

6.4.1.2.5. Cladding mode stripper

A cladding mode stripper encourages the conversion of cladding modes to radiation modes; as a result, cladding modes are stripped from the fibre.

6.4.1.2.6. Optical detector

A suitable detector shall be used so that all of the radiation emerging from the fibre is intercepted. The spectral response should be compatible with spectral characteristics of the source. The detector must be uniform and have linear sensitivity characteristics.

6.4.1.3. Measurement procedure

6.4.1.3.1. Preparation of fibre under test

Fibre ends shall be substantially clean, smooth and perpendicular to the fibre axis. Measurements on uncabled fibres shall be carried out with the fibre loose on the drum, i.e., microbending effects shall not be introduced by the drum surface.

6.4.1.3.2. Procedure

1) The fibre under test is placed in the measurement set-up. The output power P_2 is recorded.
2) Keeping the launching conditions fixed, the fibre is cut to the cut-back length (for example, 2 m from the launching point). The cladding mode stripper, when needed, is refitted and the output power P_1 from the cut-back length is recorded.
3) The attenuation of the fibre, between the points where P_1 and P_2 have been measured, can be calculated, using P_1 and P_2, from the definition Equation (3-4) and Equation (3-5).

6.4.1.4. Presentation of the results

The following details shall be presented:

a) test set-up arrangement, including source type, source wavelength, and line width (FWHM);
b) fibre identification;
c) length of sample;
d) description of high-order modes filter;
e) attenuation of the sample quoted in dB;
f) attenuation coefficient quoted in dB/km;
g) indication of accuracy and repeatability;
h) temperature of the sample and environmental conditions (if necessary).

6.4.2. First alternative test method: The backscattering technique

6.4.2.1. General

A test method for the attenuation coefficient of single-mode optical fibre based on bidirectional backscattering measurements is described. This technique can also be applied to check the attenuation uniformity, optical continuity, physical discontinuities, splice losses and the length of the fibre.

Unidirectional backscattering measurements can be adopted in particular cases, e.g., verification of the backscatter slope variation in cabled fibres.

Procedures for the calibration of backscattering equipment (for single-mode fibres) are provided in [IEC 61746-1].

6.4.2.2. Test apparatus

6.4.2.2.1. General considerations

The signal level of the backscattered optical signal will normally be small and close to the noise level. In order to improve the signal-to-noise ratio and the dynamic measuring range, it is therefore customary to use a high power light source in connection with signal processing of the detected signal. In addition, adjustment of the pulse width may be required to obtain a compromise between resolution and dynamic range.

Care must be taken that higher order modes do not propagate.

An example of apparatus is shown in Figure 14-a.

6.4.2.2.2. Optical source

Use a stable, high power optical source of appropriate wavelengths and record them. The pulse width and repetition rate should be consistent with the desired resolution and the length of the fibre.

6.4.2.2.3. Optical coupling system

An optical system for an efficient coupling of the beam into the fibre under test, the branching device or the optical detector shall be used. Various devices, such as index matching materials, can be added to reduce Fresnel reflections.

6.4.2.2.4. Branching device

A branching device is needed to couple the source radiation into the fibre and the backscattered radiation onto the detector, while avoiding a direct source-detector coupling. Avoid using devices with polarization-dependent properties.

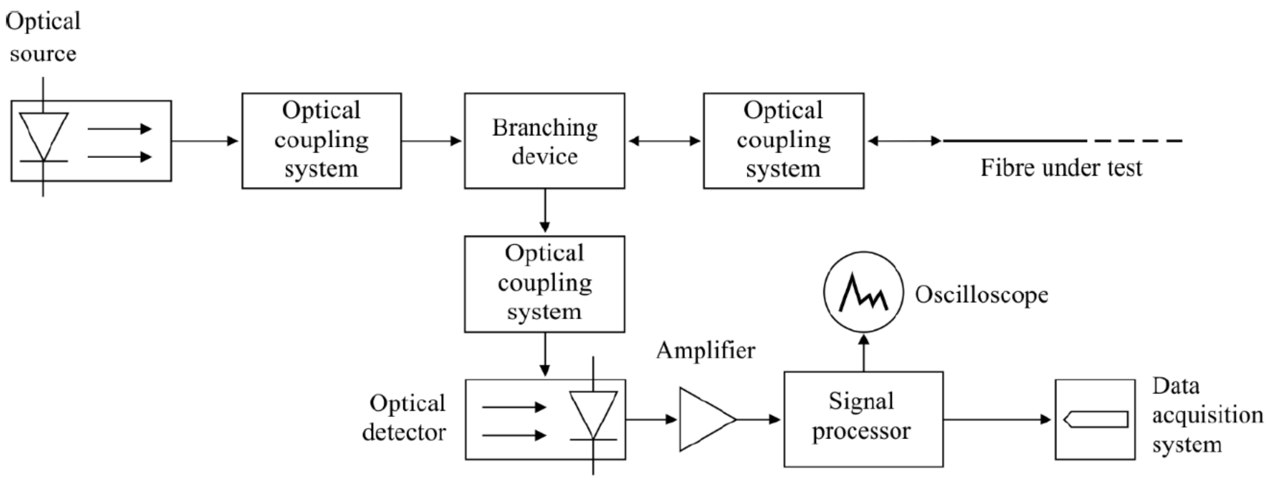


Figure 14-a — Schematic of apparatus

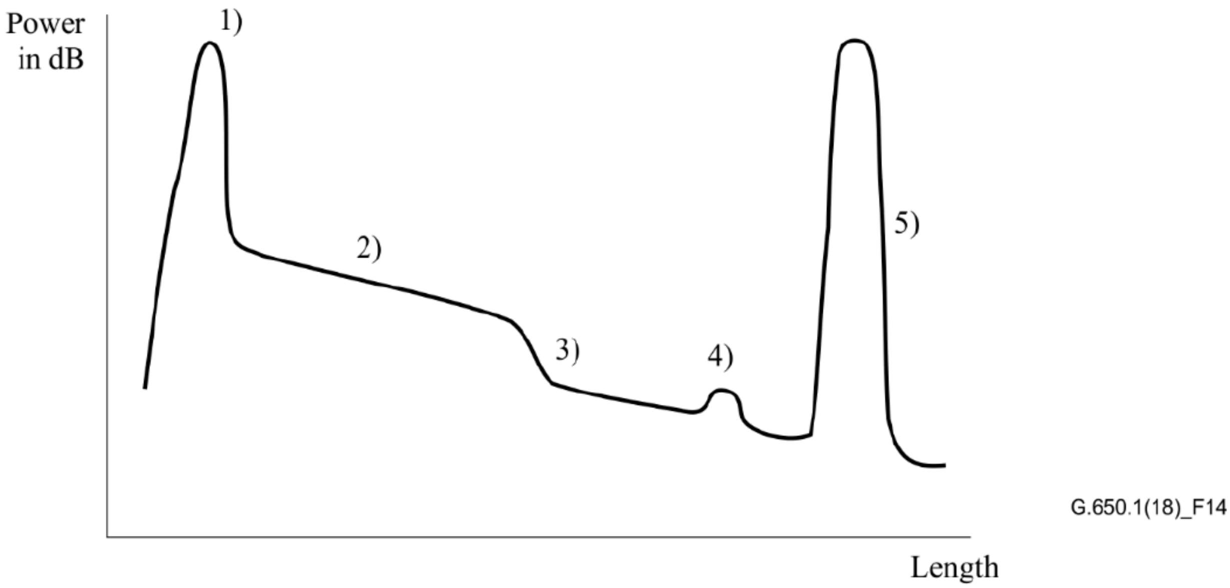


Figure 14-b — Example of a undirectional backscattering loss curve

Figure 14 — The backscattering technique

6.4.2.2.5. Optical detector

A detector shall be used so that the maximum possible backscattered power is intercepted. The detector response shall be compatible with the levels and wavelengths of the detected signal. A substantially linear detector response is required for attenuation measurements.

6.4.2.2.6. Amplifier

A suitable amplifier shall follow the optical detector, so that the signal level becomes adequate for signal processing. The amplifier bandwidth should involve a trade-off between time resolution and noise reduction.

6.4.2.2.7. Signal processor

A signal processor able to improve the signal-to-noise ratio, to calculate the attenuation curve from the two unidirectional backscattering loss curves, and to provide a logarithmic response in the detection system is required. An oscilloscope for a direct view of the backscattering trace and a data acquisition system to store the measurement results can be connected to the signal processor.

6.4.2.2.8. Cladding mode stripper

See clause 6.4.1.2.5

6.4.2.2.9. Fibre sample configuration

The measurement may be made with the fibre in a number of fibre configurations (e.g., as cabled fibre, on a suitable shipping spool or as required for the reference text method).

6.4.2.3. Measurement procedure

a) Align the fibre under test to the optical coupling system.

b) Measure two unidirectional backscattering loss curves, one from each end of the fibre. Figure 14-b shows an example of such a unidirectional curve. Each backscattering loss curve is analysed by the signal processor and recorded on a logarithmic scale, avoiding the parts at the two ends of the curves, due to the reflections of the coupling and branching devices and by the fibre ends (see parts 1) and 5) in Figure 14-b.

c) Evaluate the length, L_f, of the fibre from the time interval between the two ends of the backscattering loss curve, T_f, and the group delay index, N, of the fibre as: $L_f = c \cdot T_f / N$ (c being the free space light speed).

d) Obtain the bidirectional backscattering loss curve using the two measured and recorded unidirectional backscattering loss curves, according to the procedure outlined in the following:
Let a(x) and b(z) be the functions describing the two unidirectional backscattering loss curves expressed in dB, with x and z being the distances from the fibre ends nearest the respective launch site. The bidirectional backscattering loss curve is given by:

$$y(x) = \frac{a(x) - b(L_f - x)}{2} \qquad \text{(6-14)}$$

e) Obtain the end-to-end fibre attenuation coefficient according to the procedure outlined in the following:
The attenuation coefficient, $A(x_0, x_1)$, for a fibre segment defined by the end positions x_0 and x_1 (with $x_0 < x_1$) is given by:

$$A(x_0, x_1) = \frac{y(x_0) - y(x_1)}{x_1 - x_0} \qquad \text{(6-15)}$$

This expression may be evaluated by a least squares linear fit of the data between x_0 and x_1.
The end-to-end fibre attenuation coefficient is determined in the same way as Equation (6-15) with the data points as close as possible to the end positions. However, these points should be outside the dead zone area and the end reflection area (see Figure 14-b, areas 1) and 5)).

6.4.2.4. Presentation of the results

The following details shall be presented:

a) test set-up arrangement;
b) kind of signal processing used;
c) date of test;
d) test specimen identification and length;
e) pulse width;
f) test wavelength(s);
g) end-to-end fibre attenuation coefficient in dB/km;
h) bidirectional backscattering loss curve.

NOTE – Unidirectional backscattering measurements are obtained with the function a(x) alone. The complete analysis of the recorded unidirectional backscattering loss curves (Figure 14-b) shows that, independently from the attenuation measurements, many phenomena can be monitored using the backscattering technique including:

1) reflection originated by the branching and coupling devices at the input end of the fibre;
2) zone of invariant backscattered slope;
3) discontinuity due to local defect, splice or coupling;
4) backscattering slope variation with length;
5) fluctuation at the output end of the fibre;
6) attenuation change, for example, with temperature.

6.4.3. Second alternative test method: The insertion loss technique

6.4.3.1. General

The insertion loss technique consists of the evaluation of the power loss due to the insertion of the fibre under test between a launching and a receiving system, previously interconnected (reference condition). The powers P_1 and P_2 are thus evaluated in a less straightforward way than in the cut-back method. Therefore, this method is not intended for use on factory lengths of fibres and cables.

The insertion loss technique is less accurate than a cut-back one, but has the advantage of being non-destructive for the fibre under test and for the semi-connectors possibly fixed at both ends. Therefore, it is particularly suitable for field use, and mainly intended for use with connectorized cable lengths.

Two options are considered in the following for this technique (see Figure 15); they differ in the nature of the launching and receiving systems, as outlined below. Measurement conditions in between option a) and b) are possible and are discussed in Note 2 in clause 6.4.3.3.2.

In option a), the quality of the semi-connectors possibly fixed to the fibre under test (and in general the quality of the used interconnection devices) influences the results; in option b), this influence is nearly excluded. As a consequence, option b) has in general a better accuracy, and it is more suitable when the actual attenuation of the fibre alone is needed. Conversely, when the fibre section under test is fitted with semi-connectors and has to be cascaded with other elements, the results from option a) are more meaningful, as they take into account the deviation of the semi-connectors from the nominal loss.

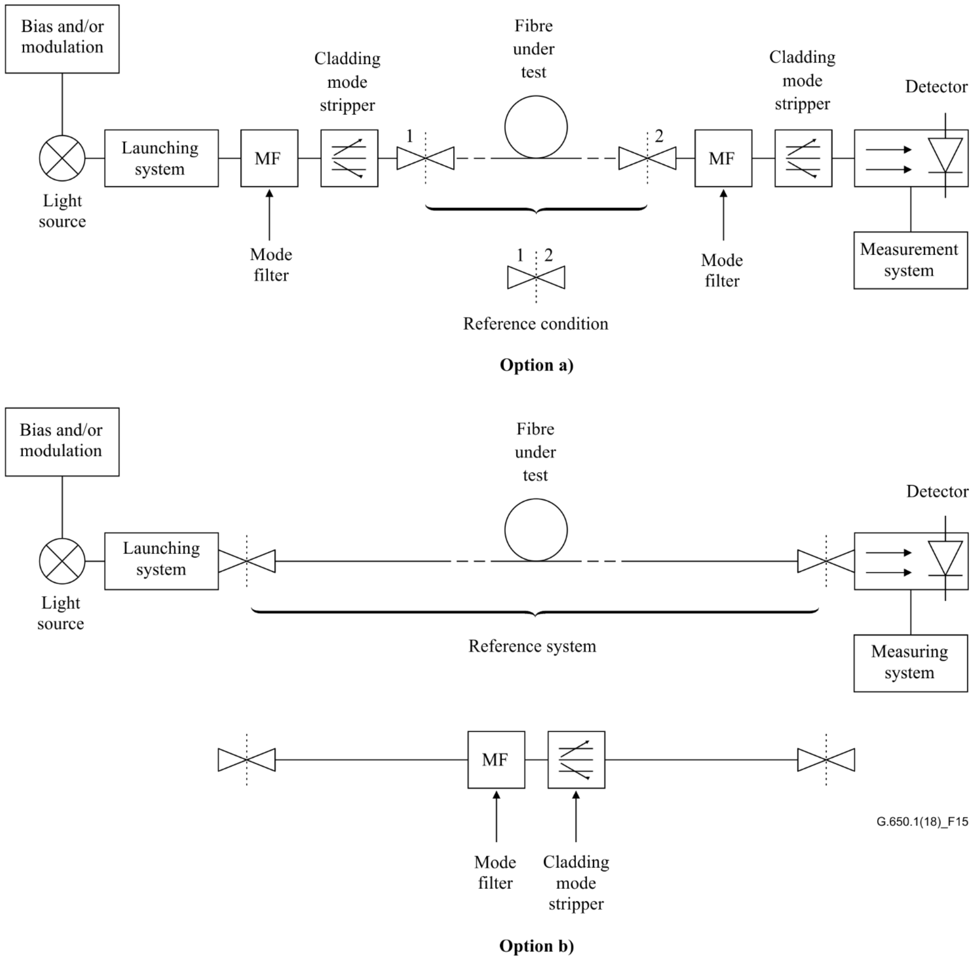


Figure 15 — Typical arrangements for the insertion loss technique

6.4.3.2. Test apparatus

The schematic diagram of the test apparatus is shown in Figure 15. Measurements may be made at one or more wavelengths, or alternatively, a spectral response may be required over a range of wavelengths.

6.4.3.2.1. Optical source

A suitable intensity stable radiation source shall be used, such as a lamp, a laser or a light emitting diode. If a broad spectrum source is used, it should be followed by a wavelength selection device (alternatively this device can be inserted before the detector). In every case, the nominal wavelength of the source (possibly taking into account the wavelength selection device) shall be known.

The spectral width (FWHM) should be narrow compared with any features of the fibre spectral attenuation.

6.4.3.2.2. Modulation

See clause 6.4.1.2.2.

6.4.3.2.3. Launching conditions

For option a)

The source is coupled to a short length of single-mode fibre having the same nominal characteristics of the fibre under test and equipped with a mode filter and a cladding mode stripper (see below).

The above single-mode fibre is coupled to the fibre under test with a very precise coupling device to minimize coupling losses and ensure meaningful results. If the fibre under test is equipped with a semi-connector, a compatible high quality semi-connector shall be fixed to the launching fibre.

For option b)

The source is coupled through a suitable optic to the fibre under test in such a way that the launched spot at the fibre input-end face has a near-field and a far-field intensity almost uniform within the mode field diameter and the far-field intensity of the fibre under test.

The system can employ lenses and a fibre positioner; alternatively, the light can be launched in a step-index multimode fibre to be connected to the fibre under test.

This is accomplished with any coupling device or a semi-connector compatible with those terminating the fibre under test.

6.4.3.2.4. Reference system (option b) only)

This system is composed of a short length of single-mode fibre having the same nominal characteristics of the fibre under test. The fibre is equipped with a mode filter and a cladding mode stripper; both devices shall not introduce any loss on the fundamental mode.

6.4.3.2.5. Mode filter

The mode filter shall allow the propagation along the fibre of the fundamental mode only. It can be implemented by a suitable bending condition on the fibre. For example, a one-turn bend with a radius of 30 mm on the fibre is generally sufficient for most ITU-T G.65x fibres. For some [ITU-T G.657] fibres, a smaller radius, multiple bends or longer sample lengths can be applied to remove high-order propagating modes.

6.4.3.2.6. Cladding mode stripper

A cladding mode stripper encouraging the conversion of cladding modes to radiation modes should be employed. This device is not necessary if the fibre itself does not allow the propagation cladding modes.

6.4.3.2.7. Optical detection

The spectral response of the optical detector shall be compatible with the spectral characteristics of the source. It must have linear sensitivity characteristics.

For option a)

The detector is connected to a single-mode fibre having the same nominal characteristics of the fibre under test. The fibre should be equipped with a mode filter and a cladding mode stripper.

For the coupling with the fibre under test, the same indication as in clause 6.4.3.2.3, option a), is used.

For option b)

The end of the fibre under test is positioned in front of the detector.

A suitable detector shall be used so that all the radiation emerging from the fibre is intercepted. The detector should be spatially uniform.

Alternatively, the detector is connected to a step-index multimode fibre. This fibre is coupled to the fibre under test by any coupling device or a semi-connector compatible with those terminating the fibre under test.

6.4.3.3. Measurements procedure

6.4.3.3.1. Preparation of fibre under test

See clause 6.4.1.3.1.

If the fibre is fitted with connectors, an appropriate cleaning procedure is required.

6.4.3.3.2. Procedure

1) Once a measurement wavelength is selected, the power P_1 is firstly measured in the following way:

   For option a)
   The fibre of the launching system is connected to the fibre of the receiving system. The received power P_1 is then recorded.

   For option b)
   The reference system is connected between the launching and the receiving systems. The received power P_1 is then recorded.

2) Successively, the fibre under test is connected between the launching and the receiving systems. The received power P_2 is then recorded.

3) Finally, the attenuation A of the fibre section is calculated in the following way:

For option a)

$$A = 10\log\frac{P_1(\lambda)}{P_2(\lambda)} + C_r - C_1 - C_2(dB) \qquad (6\text{-}16a)$$

where C_r, C_1, and C_2 are the nominal average losses (in dB) of the connections respectively in the reference conditions at the input of the fibre under test and at its output.

For option b)

$$A = 10\log\frac{P_1(\lambda)}{P_2(\lambda)}(dB) \qquad (6\text{-}16b)$$

NOTE 1 –

The use of option b) assumes that the fibre under test does not allow the propagation to the receiving end of modes other than the fundamental one.

NOTE 2 –

Fibre attenuation measurements are also possible with a hybrid test set-up, using a launching system as in option a) and a receiving system as in option b), or vice versa.

The measurement procedure for P_1 is in both cases similar to the one listed above for option a); no reference system is required and the launching system is connected directly to the receiving system.

In both cases the fibre section attenuation can be calculated as:

$$A = 10\log\frac{P_1(\lambda)}{P_2(\lambda)} - C_a(dB) \qquad (6\text{-}17)$$

where C_a is the nominal average loss (in dB) of the connection between the fibre under test and that part of the test set-up (launch or receive) belonging to option a).

NOTE 3 –

The intrinsic capability of option a) to evaluate the semi-connectors behaviour does not imply its use whenever this evaluation is required.

Alternative possibilities are in using, even at an end where the semi-connector evaluation is required, an option b) set-up, previously connecting a single-mode cord to the fibre under test. The nominal loss of the fibre-to-cord connector is to be subtracted from the measured loss.

The test apparatus to be used in practice should be chosen to minimize the error sources, taking into account the available instrumentation and connecting devices. The use of a hybrid set-up (a-launch, b-receive) plus a cord at the receiving end is usually the best solution when both the semi-connectors have to be evaluated.

6.4.3.4. Presentation of the results

The following details shall be presented:

a) test set-up arrangement, including source type, source wavelength, spectral width (FWHM) used for the measurement and the option type a) or b);
b) fibre identification;
c) length of the fibre section and end conditions (presence of semi-connectors);
d) description of high-order modes filter;
e) attenuation of the section quoted in dB;
f) attenuation coefficient quoted in dB/km;
g) indication of accuracy and repeatability (the connection loss repeatability shall be taken properly into account);
h) temperature of the sample and environmental conditions (if necessary).

6.4.4. Third alternative test method: Spectral attenuation modelling

6.4.4.1. General

The attenuation coefficient of a fibre across a spectrum of wavelengths may be calculated by means of a characterizing matrix, M, and a vector, v. The vector contains the measured attenuation coefficients of a small number (three to five) of wavelengths (e.g., 1310 nm, 1360 nm, 1380 nm, 1410 nm, 1550 nm, and/or 1625 nm).

In one approach, the fibre or cable supplier shall provide a matrix characteristic of its product, and the modelled spectral attenuation is a vector, w, calculated from the product of M and v:

$$w = M \cdot v$$

Alternatively, if using a generic matrix, the supplier shall provide a correction-factor vector so that the prediction equation becomes:

$$W = w + e$$

where::

W	is the modified vector
w	comes from $w = M \cdot v$
e	is the correction-factor vector

A generic matrix is a characterizing matrix which can be applied to a variety of fibres, designs and suppliers (presumably within a single fibre type), and which is determined and/or invoked by a standards body, single customer/end-user, or other industry source to which individual suppliers can compare their products, the difference being resolved by the vector, e.

6.4.4.2. Test apparatus

Since this technique involves a calculation using previously determined values, there is no specific apparatus required. Any of the recommended test methods (clause 6.4.1 the cut-back technique; clause 6.4.2 the backscattering technique; clause 6.4.3 the insertion loss technique) may be used to generate the measured values upon which the calculations are made.

Direct measurements of attenuation take precedence over this method and is a case of conflict.

6.4.4.3. Calculation procedure

The attenuation coefficient of a fibre across a spectrum of wavelengths may be calculated from $w = M \cdot v$. The vector, v, contains the measured attenuation coefficients of a small number (three to five) of predictor wavelengths (e.g., 1310 nm, 1360 nm, 1380 nm, 1410 nm, 1550 nm, and/or 1625 nm) which were measured using one of the previous attenuation test methods. Multiplying the matrix, M, times the vector, v, yields another vector, w, which contains the predicted attenuation coefficients at many wavelengths (such as at 10 nm wavelength intervals from 1240 nm to 1600 nm).

The matrix, M, is given by:

$$\begin{bmatrix} A_{11} & A_{12} & \dots & A_{1n} \\ A_{21} & A_{22} & \dots & A_{2n} \\ \vdots & \vdots & \vdots & \vdots \\ A_{m1} & A_{m2} & \dots & A_{mn} \end{bmatrix}$$

where m is the number of wavelengths where the attenuation coefficients have to beestimated, and n is the number of predictor wavelengths. An example of such a matrix is given for illustrative purposes in Appendix III.

The standard deviation of the difference between the actual and predicted attenuation coefficients at each wavelength is to be less than 0,xx dB/km within a stated wavelength range. A different tolerance – 0,yy dB/km – may be necessary if an additional wavelength range is specified. The values of xx and (yy), and the wavelength range(s) should be agreed upon between the user and the manufacturer.

If the estimate is obtained by using the supplier's specific matrix, M, then no correction vector, e, is necessary.

Since the elements of both M and e are achieved on a statistical basis, the w vector elements shall be determined as statistical. To indicate the accuracy of the predicted attenuation coefficients, the fibre suppliers shall give a vector containing the standard deviation of the differences between the actual and predicted attenuation coefficients, together with M and/or e (see clause 6.4.4.4).

NOTE 1 – In order to facilitate use of this matrix, the fibre should be routinely measured at the predictor wavelengths. The predictor wavelengths should number from 3 to 5, with a strong preference given to the lower number if sufficient accuracy can be achieved.

NOTE 2 – This model considers only uncabled fibre attenuation. An additional vector must be added to w to take account of cabling effects and environmental effects.

6.4.4.4. Presentation of the results

In addition to the items to be reported for the test method used in measuring the attenuation coefficients, report the following items:

a) the predicted attenuation and corresponding wavelength;
b) the method used to obtain the measured attenuation coefficient values (if requested);
c) the matrix used to predict the spectral attenuation, or the correction vector if a standard matrix was used (if requested);
d) the vector containing the standard deviation of the differences between the actual and predicted attenuation coefficients obtained during the development of the matrix (if requested).

6.5. Test methods for chromatic dispersion

Chromatic dispersion varies with wavelength. Some methods and implementations measure the group delay as a function of wavelength and the chromatic dispersion and dispersion slope are deduced from the derivatives (with respect to wavelength) of this data. This differentiation is most often done after the data has been fitted to a mathematical model. Other implementations of the reference method can allow direct measurement at each of the required wavelengths.

For some categories of fibre the chromatic dispersion attributes are specified with the parameters of a specific model. In these cases the relevant Recommendation defines the model appropriate for the definition of the specified parameters. For other fibre categories, the dispersion is specified to be within a given range for one or more specified wavelength intervals. In the latter case, either direct measurements may be made at the wavelength extremes or a fitting model may be used to either allow group delay measurement methods or implementations, or to allow the storage of a reduced set of parameters that may be used to calculate the interpolated dispersion for particular wavelengths which may not have actual direct measurement values.

Annex A gives a general description of chromatic dispersion fitting and outlines a number of fitting equations suitable for use with any of the measurement methods or fibre categories.

Appendix V gives the interferometric technique for chromatic dispersion measurement.

6.5.1. Reference test method: The phase-shift technique

6.5.1.1. General

The fibre chromatic dispersion coefficient is derived from the measurement of the relative group delay experienced by the various wavelengths during propagation through a known length of fibre.

The group delay is measured in the frequency domain, by detecting, recording and processing the phase shift of a sinusoidal modulating signal.

The chromatic dispersion may be measured at a fixed wavelength or over a wavelength range.

NOTE – Differential phase shift is documented in [IEC 60793-1-42], Annex C.

6.5.1.2. Test apparatus

Aschematic diagram of the test apparatus is shown in Figure 16.

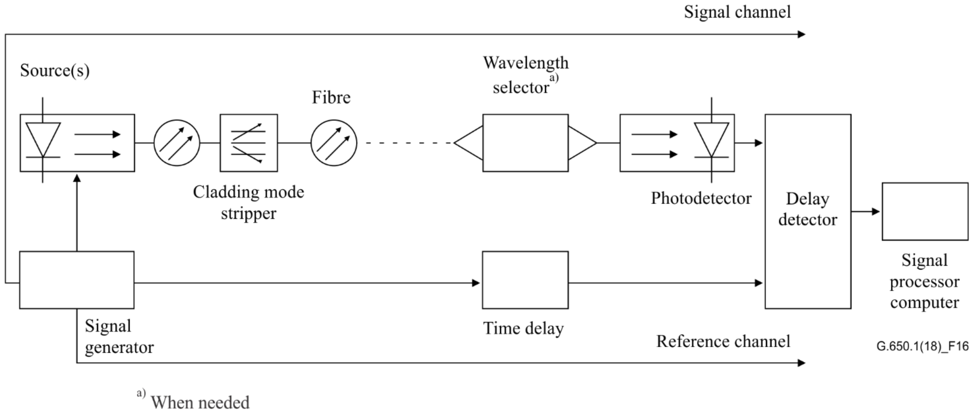


Figure 16 — Typical arrangement of the test apparatus

6.5.1.2.1. Optical source

The optical source shall be stable in position, intensity and wavelength over a time period sufficiently long to complete the measurement procedure. Laser diodes, (laser diode array (LD-array)), wavelength tunable laser diodes (WTL) (e.g., an external cavity laser (ECL)), LEDs or broadband sources, (e.g., an Nd:YAG laser with a Raman fibre) may be used, depending on the wavelength range of the measurement.

In any case, the modulating signal shall be such as to guarantee a sufficient time resolution in the group delay measurement.

6.5.1.2.2. Wavelength selection

The wavelength selector and monitoring are used to select and monitor the wavelength at which the group delay is to be measured. As a wavelength selector, an optical switch, a monochromator, dispersive devices, optical filters, optical couplers, connectors may be used, depending on the type of light sources and measurement set-up. The selection may be carried out by switching electrical driving signals for different wavelength light sources.

The wavelength monitoring may be carried out by an optical fibre coupler and a wavelength meter. The wavelength selector and monitor may be used either at the input or at the output end of the fibre under test.

If a mathematical fit is made to the data, at least one data point must be within 100 nm of λ_0.

6.5.1.2.3. Detector

The light emerging from the fibre under test, the reference fibre or the optical divider, etc., is coupled to a photodetector whose signal-to-noise ratio and time resolution are adequate for the measurement. The detector is followed by a low noise amplifier if needed.

6.5.1.2.4. Reference channel

The reference channel may consist of an electrical signal line or optical signal line. A suitable time delay generator may be interposed in this channel. In certain cases, the fibre under test itself can be used as the reference channel line.

6.5.1.2.5. Delay detector

The delay detector shall measure the phase shift between the reference signal and the channel signal. A vector voltmeter could be used.

6.5.1.2.6. Signal processor

A signal processor can be added in order to reduce the noise and/or the jitter in the measured waveform. If needed, a digital computer can be used for purposes of equipment control, data acquisition and numerical evaluation of the data.

6.5.1.3. Measurement procedure

The fibre under test is suitably coupled to the source and to the detector through the wavelength selector or the optical divider, etc. If needed, a calibration of the chromatic delay of the source may be performed. A suitable compromise between wavelength resolution and signal level must be achieved. Unless the fibre under test is also used as the reference channel line, the temperature of the fibre must be sufficiently stable during the measurement.

The phase shift between the reference signal and the channel signal at the operating wavelength are to be measured by the delay detector. Data processing appropriate to the type of modulation is used in order to obtain the chromatic dispersion coefficient at the operating wavelength. When needed, a spectral scan of the group delay versus wavelength can be performed; from the measured values a fitting curve can be completed.

The time group delay will be deduced from the corresponding phase shift φ through the relation $\tau=\varphi/(2\pi f)$, f being the modulation frequency.

6.5.1.4. Presentation of the results

The following details shall be presented:

a) test set-up arrangement;
b) type of modulation used;
c) source characteristics;
d) fibre identification and length;
e) characteristics of the wavelength selector (if present);
f) type of photodetector;
g) characteristics of the delay detector;
h) model used to fit the relative group delay data or chromatic dispersion data, and the fitting wavelength range used;
i) values of coefficients from the fit for each fitting wavelength range;
j) temperature of the sample and environmental conditions (if necessary).

6.5.2. Alternative test method: The pulsedelay technique

6.5.2.1. General

The fibre chromatic dispersion coefficient is derived from the measurement of the relative group delay experienced by the various wavelengths during propagation through a known length of fibre.

The group delay is measured in the time domain, by detecting, recording and processing the delay experienced by pulses at various wavelengths.

The chromatic dispersion may be measured at a fixed wavelength or over a wavelength range.

6.5.2.2. Test apparatus

A schematic diagram of the test apparatus is shown in Figure 16.

6.5.2.2.1. Optical source

The optical source shall be stable in position, intensity and wavelength over a time period sufficiently long to complete the measurement procedure. Laser diodes, (laser diode array (LD-array)), wavelength tunable laser diodes (WTL) (e.g.,an external cavity laser (ECL)), broadband sources (e.g., an Nd:YAG laser with a Raman fibre) may be used, depending on the wavelength range of the measurement.

In any case, the modulating signal shall be such as to guarantee a sufficient time resolution in the group delay measurement.

6.5.2.2.2. Wavelength selection

A wavelength selector and monitoring are used to select and monitor the wavelength at which the group delay is to be measured. As a wavelength selector, an optical switch, a monochromator, dispersive devices, optical filters, optical couplers, connectors may be used, depending on the type of light sources and measurement set-up. The selection may be carried out by switching electrical driving signals for different wavelength light sources.

The wavelength monitoring may be carried out by an optical fibre coupler and a wavelength meter. The wavelength selector and monitor may be used either at the input or at the output end of the fibre under test.

If a mathematical fit is made to the data, at least one data point must be within 100 nm of the zero-dispersion wavelength λ_0.

6.5.2.2.3. Detector

The light emerging from the fibre under test, the reference fibre or the optical divider, etc., is coupled to a photodetector whose signal-to-noise ratio and time resolution are adequate for the measurement. The detector is followed by a low noise amplifier if needed.

6.5.2.2.4. Reference channel

The reference channel may consist of an electrical signal line or optical signal line. A suitable time delay generator may be interposed in this channel. In certain cases, the fibre under test itself can be used as the reference channel line.

6.5.2.2.5. Delay detector

The delay detector shall measure the delay time between the reference signal and the channel signal. A high-speed oscilloscope or a sampling oscilloscope could be used.

6.5.2.2.6. Signal processor

A signal processor can be added in order to reduce the noise and/or the jitter in the measured waveform. If needed, a digital computer can be used for the purposes of equipment control, data acquisition and numerical evaluation of the data.

6.5.2.3. Measurement procedure

The fibre under test is suitably coupled to the source and to the detector through the wavelength selector or the optical divider, etc. If needed, a calibration of the chromatic delay of the source may be performed. Asuitable compromise between wavelength resolution and signal level must be achieved. Unless the fibre under test is also used as the reference channel line, the temperature of the fibre must be sufficiently stable during the measurement.

The time delay between the reference signal and the channel signal at the operating wavelength are to be measured by the delay detector. Data processing appropriate to the type of modulation is used in order to obtain the chromatic dispersion coefficient at the operating wavelength. When needed, a spectral scan of the group delay versus wavelength can be performed; from the measured values a fitting curve can be completed.

6.5.2.4. Presentation of the results

The following details shall be presented:

a) test set-up arrangement;
b) type of modulation used;
c) source characteristics;
d) fibre identification and length;
e) characteristics of the wavelength selector (if present);
f) type of photodetector;
g) characteristics of the delay detector;
h) model used to fit the relative group delay data or chromatic dispersion data, and the fitting wavelength range used;
i) values of coefficients from the fit for each fitting wavelength range;
j) temperature of the sample and environmental conditions (if necessary).

6.6. Test methods for macrobend loss

6.6.1. Reference test method: Fibre winding

6.6.1.1. General

The macrobending loss measurement is intended to provide a means whereby certain loss values under different curvature radii are used to evaluate the macrobending performance of single-mode fibres.

NOTE – A "curvature radius" is defined as the radius of the suitable circular shaped support (e.g., mandrel or guiding groove on a flat surface) on which the fibre can be bent.

6.6.1.2. Measurement considerations

6.6.1.2.1. Sample length

The specimen shall be a known length of fibre, as specified in the detailed specification. In particular, the length of the sample tested for loss is determined by the measurement set-up, i.e., curvature radius (R) and number of turns (N); any further fibre length does not affect the measurement results, provided that the signal-to-noise (S/N) ratio is optimized.

6.6.1.2.2. Number of coils

The number of coils should be in accordance with the values stated in the relevant [ITU-T G.652], [ITU-T G.653], [ITU-T G.654], [ITU-T G.655], [ITU-T G.656] and [ITU-T G.657].

For single-mode fibres, the attenuation increases in a linear fashion with the number of coils.

For each radius, the number of coils shall be chosen in such a way that:

a) the induced loss is significantly higher than the detection limit of the set-up; when necessary, e.g., for low-bend loss fibres, tests may be carried out with more coils than the specification requires, followed by linear normalization to the specified number;

b) the induced loss is significantly lower than the onset of the non-linear region in the set-up; for bending radii in the range 5 to 10 mm this may imply that not more than 5 to 10 coils should be used.

6.6.1.2.3. Bend radius

The value of bend radius shall be in accordance with the values stated in the relevant [ITU-T G.652], [ITU-T G.653], [ITU-T G.654], [ITU-T G.655], [ITU-T G.656] and [ITU-T G.657]. It should be considered that the macrobending losses increase exponentially as radius decreases.

NOTE – Further information on the relationship between macrobending losses and radius can be found in Annex A of [IEC 60793-1-47 RLV].

6.6.1.2.4. Measurement wavelength

The measurement wavelength shall be 1550 nm or 1625 nm, in accordance with the relevant [ITU-T G.652], [ITU-T G.653], [ITU-T G.654], [ITU-T G.655], [ITU-T G.656] and [ITU-T G.657]. It should be considered that macrobending losses increase exponentially with the wavelength.

NOTE 1 – As optical bending losses of single-mode fibres increase with wavelength, a loss specification at the highest envisioned wavelength, i.e., either 1550 or 1625 nm, is suffice. If required, customer and supplier can agree on a lower or higher specification wavelength.

NOTE 2 – Further information on the relationship between macrobending losses and measurement wavelength can be found in Annex A of [IEC 60793-1-47 RLV].

NOTE 3 – Further information on approximating bend loss for single-mode fibres across a broad wavelength range at various effective bends can be found in Annex E of [IEC 60793-1-47 RLV].

6.6.1.3. Test apparatus

The apparatus consists of a bending tool and a loss-measurement instrument.

6.6.1.3.1. Bending tool

The bending tool is used to hold the sample bent with a radius as stated in the specification. A mandrel or a guiding groove on a flat surface is applicable.

Since the actual curvature radius is critical, a maximum tolerance of ± 0.1 mm (for radii lower than or equal to 15 mm) or ± 0.5 to 1.0 mm (for larger radii) is accepted (a tighter tolerance on small radii is required for the higher measurement sensibility).

The test can be carried out on samples either making complete (360°) turn(s) in open air or around a suitable support (mandrel), or making u-turn(s) (180°) in open air or around suitable supports; the length under test is different in the two configurations, the length of a complete turn being twice the length of a u-turn. In the following, the term "coil" refers to one complete turn: one "coil" is made by two consecutive "u-turns" 3. This should be taken into account when normalizing the results to the length of the sample (number of coils).

6.6.1.3.2. Loss measurement instrument

The loss-measurement instrument uses either the transmitted power monitoring technique (methodA of [IEC 60793-1-46]) or the cut-back technique (as in clause 6.4.1), taking care of the appropriate launch condition for the specific fibre type.

6.6.1.4. Measurement procedure

Prepare a flat end face, orthogonal to the fibre axis, at the input and output ends of each test specimen.

Loosely wind the fibre on the tool, avoiding excessive fibre twist. The number of turns, curvature radius and wavelength at which loss is to be measured are discussed in the following paragraphs.

Optical powers can be measured in the following two ways:

a) the power-monitoring technique, which measures the fibre attenuation increase due to a change from the straight condition to a bent condition; or
b) the cut-back technique, which measures the total attenuation of the fibre in the bent condition. In order to determine the induced attenuation due to macrobending, this value should be corrected for the intrinsic attenuation of the fibre.

The fibre length outside the mandrel and the reference cut-back length shall be free of bends that might introduce a significant change in the measurement result. Collection of excess fibre in a bend radius of at least 140 mm is recommended.

It is also possible to rewind the fibre from a mandrel with a large radius (introducing negligible macrobend loss) to the mandrel with the required radius. In this case, the macrobend loss can be determined directly by using the power-monitoring technique (without the correction for the intrinsic attenuation of the fibre).

Care must be taken in order not to introduce torsion on any fibre part during the measurements, as this would affect the result.

NOTE – Whispering gallery mode caused by reflection of radiating mode at cladding-coating or coating-air interface may affect the macrobending loss measurement. For example, multiple fibre coils or coated/stripped fibre coil immersed with adequate refractive index liquid may be used to reduce the interference.

6.6.1.4.1. Calculation

The results are reported in dB as:

$$Loss(dB) = 10\log_{10}\frac{P_{str}}{P_{bend}} \qquad (6\text{-}18)$$

where P_{str} is the power measured without the bend and P_{bend} is the power measured with the bend present.

6.6.1.5. Presentation of the results

The following details shall be presented:

a) test set-up arrangement;
b) fibre identification;
c) length of specimen;
d) macrobend radius;
e) number of coils;
f) wavelength(s) of interest;
g) macrobending loss (dB) or (dB/turn).

6.7. Test methods for prooftesting

6.7.1. Reference test method: Longitudinal tension

6.7.1.1. General

a) This test method describes procedures for briefly applying tensile loads to an entire continuous length of fibre. The initial length may break into several shorter lengths, and each shorter length is considered to have passed the proof test. An informative background can be found in [b-IEC/TR 62048].

b) Proof testing is performed during fibre manufacturing, online as part of the fibre drawing and coating process, or offline as part of the testing process. A break rate (failure per unit length) is statistically expected.

c) Standard ambient environmental conditions are used for storage and proof testing: 23 ± 5°C and 50 ± 20% relative humidity. The storage time prior to proof testing is an item for further study.

d) Either stress σ or strain ε may be used in the measurement. They are related by:

$$\sigma = E_0(1+c_s\varepsilon)\varepsilon \qquad (6\text{-}19)$$

where E_0 is Young's modulus at zero stress, and c_s is a parameter (typically between 3 and 6). The determination of parameters E_0 and c_s, if needed, is an item for further study.

e) The fibre stress is calculated from the applied tension, T, as:

$$\sigma = \frac{(1-F)T}{\pi a^2} \qquad (6\text{-}20)$$

where 2a is the diameter of the glass fibre and F is the fraction of the tension borne by the coating. F is given by:

$$F = \frac{\sum_{j+1}^{n} E_j A_j}{E_g \pi a^2 + \sum_{j=1}^{n} E_j A_j} \qquad (6\text{-}21)$$

n is the number of coating layers

E_j is the modulus of the jth coating layer

A_j is the nominal cross-sectional area of the jth coating layer

E_g is the modulus of the glass fibre

NOTE 1 –

Coating moduli are typically characterized by manufacturers.

NOTE 2 –

In case of strain controlled braked capstan proof test machines, this compensation for the load sharing by the coating is not applicable.

6.7.1.1.1. Proof test parameters

a) The proof stress, σ_p, is specified to control the length of the surviving sections of the fibre. The stress applied during the proof test, σ_a, is illustrated in Figure 17. The load and unload times, t_l and t_u, and the dwell-time, t_d, are also shown. The tensile load shall be applied for as short a time as possible, yet sufficiently long to ensure the glass experiences the proof stress, typically much less than one second.

b) The applied stress shall exceed the specified proof stress at all times. The unload time shall be controlled to be less than some maximum values to be agreed between user and manufacturer to control unloading damage.

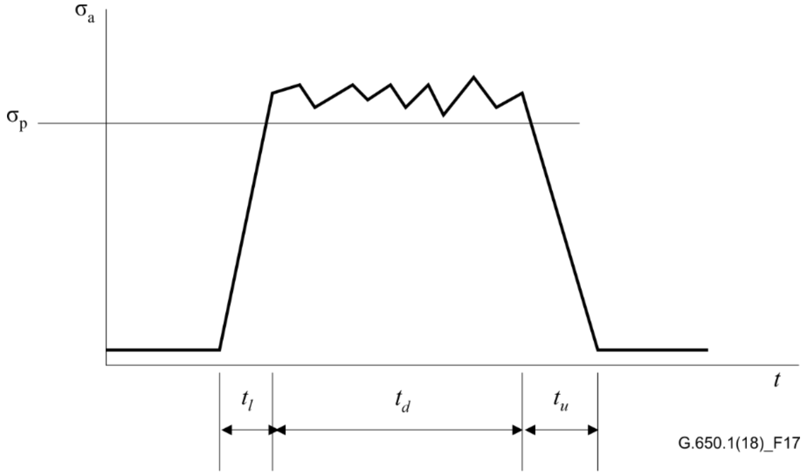


Figure 17 — Stress σ versus time t during proof testing

6.7.1.2. Test apparatus

6.7.1.2.1. Operating procedure requirements

a) In the pay-out and take-up regions, the fibre is maintained with a low value of stress typically not exceeding 10% of the proof stress (see Figure 17).

b) In the loading region, fibre stress ramps up from a low stress level to the full proof stress. The load time is t_l.

c) In the proof test region, the applied proof stress, σ_a, is maintained at values greater than the specified proof stress, σ_p.

d) In the unloading region, fibre stress ramps down from the applied stress to a low value of stress. The time to unload the fibre is t_u.

e) The unloading time is controlled to be less than a maximum value to be agreed between user and manufacturer. It can be varied by changing the processing speed or by the gripping capstan design.

f) The capstans and other support pulleys shall be designed and operated to ensure that they do not induce excessive damage. The gripping capstans shall be capable of maintaining the applied stress without inducing additional damage from slipping.

6.7.1.2.2. Proof test machines

There are several possible machine designs, all of which perform the basic functions required for measuring fibre proof with the indicated general operating requirements. Care should be used in the design so as to prevent coating damage.

Two machine types are used:
– braked-capstan machine;
– dead-weight machine.

Either machine may be used during the fibre-drawing process (online for coated fibre only), or as a separate process step (offline).

NOTE – There are dynamics with online screening, which are different from offline screening, which should be taken into account.

a) *Braked-capstan machine* (Figure 18)
The fibre is paid out with constant, low tension. Also the rewinding after the proof test is done with constant tension. The levels of the pay-off and take-up tensions are adjustable.
The proof test load is applied to the fibre between the brake and drive capstans by creating a speed difference between the capstans. Two belts are used to prevent slippage at the capstans. One design can be that the high precision tension gauge measures the load on the fibre and controls the speed difference to achieve the required proof test load. The load level and operating speed of the equipment can be independently set. Another design can be that the difference in speeds between the two capstans is set and controlled directly according to the desired fibre elongation (strain), without tension measurements.

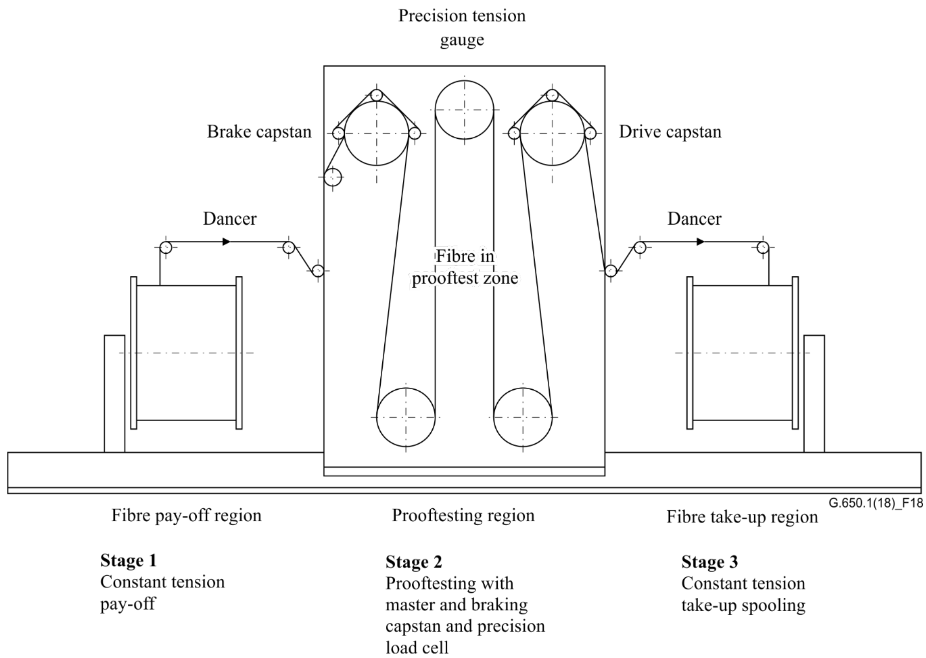


Figure 18 — Typical arrangement of a braked-capstan proof test machine

b) *Dead-weight machine* (Figure 19)
The pay-out dancer and the take-up dancer pulleys are light enough to guide the fibre with minimal tension. The pay-out capstan and the take-up capstan are synchronized with each other. The capstan pinch belts prevent slippage at the capstans, but without additional stress to the fibre or damage to the fibre coatings. A load-arm and a dead-weight on a plate are attached

to the shaft of a dead-weight dancer pulley to provide the proof stress to the fibre. An optional idler pulley provides an increased fibre gauge length if needed.

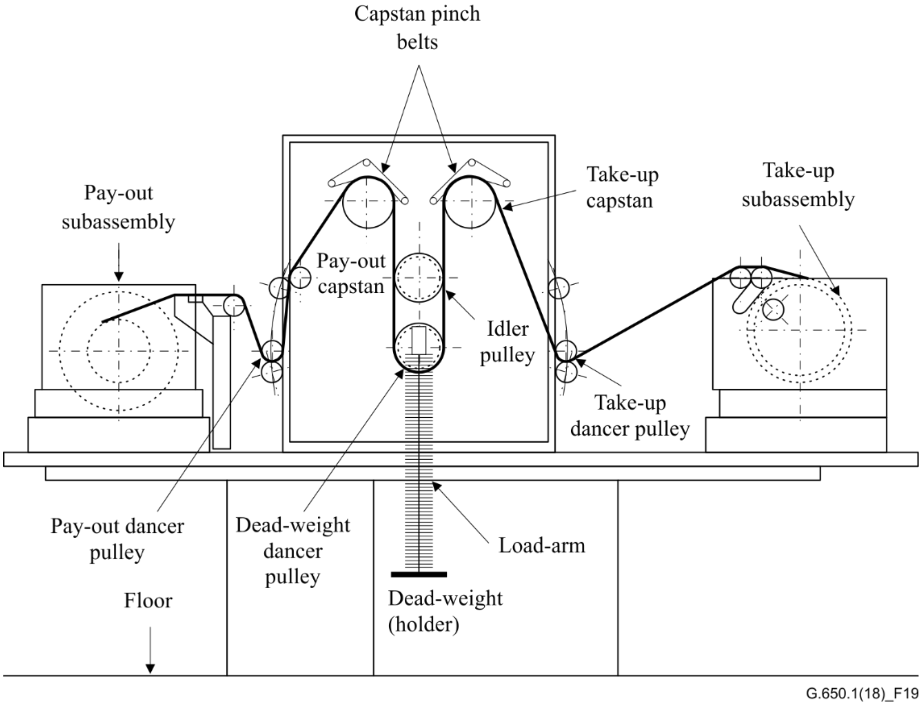


Figure 19 — Dead-weight proof test machine

6.7.1.3. Measurement procedure

6.7.1.3.1. Sample

a) The test sample shall consist of the entire length of optical fibre, minus short sections at the ends in which all requirements, i.e., maximum unloading time, may not be met. This end allowance length, typically 25 m to 50 m, shall be presented.

b) Fibre failure after proof testing shall be evidenced by complete breakage. Examination methods include visual inspection and OTDR measurements. After broken areas are removed, the surviving fibre lengths are considered to have passed the proof test procedure.

6.7.1.3.2. Calculation

If the machine is calibrated in tension, the stress is calculated from Equation (6-19). Strain may be obtained from Equation (6-18).

6.7.1.4. Presentation of the results

The following details shall be presented:

a) general description of the apparatus;
b) fibre identification;
c) average applied proof stress;
d) maximum unloading time;
e) dwell-time;
f) end allowance length.

Annex A

Chromatic dispersion fitting

(This annex forms an integral part of this Recommendation.)

A.1. General

The output from the measurement of chromatic dispersion is either directly measured chromatic dispersion values or group delay values as a function of wavelength. The chromatic dispersion value and dispersion slope is found from the derivatives of this data. The differentiation is most often done after the data has been fitted to a mathematical model.

This annex gives a general description of chromatic dispersion fitting and outlines a number of standard fitting equations.

NOTE – Even though dispersion slope characteristics may not be normative requirements, typical values are often provided by manufacturers for ease in dispersion accommodation.

A.2. Definition of equations and fitting coefficients

Table A.1 contains a general description of mathematical models that are fitted. The polynomial formulation is general and can be extended to higher order polynomials via the same principles.

Table A.2 shows the corresponding equations for dispersion slope.

Table A.3 shows the formulae for the zero-dispersion wavelength and slope at that wavelength for the 3-term Sellmeier and second-order polynomial models.

Table A.1 — Definition of fit types and fit coefficients

Fit type	Equation for group delay	Equation for dispersion data
3-term Sellmeier	$A + B \cdot \lambda^2 + C \cdot \lambda^{-2}$	$2 \cdot B \cdot \lambda - 2 \cdot C \cdot \lambda^{-3}$
5-term Sellmeier	$A + B \cdot \lambda^2 + C \cdot \lambda^{-2} + D \cdot \lambda^4 + E \cdot \lambda^{-4}$	$2 \cdot B \cdot \lambda - 2 \cdot C \cdot \lambda^{-3} + 4 \cdot D \cdot \lambda^3 - 4 \cdot E \cdot \lambda^{-5}$
2nd order polynomial (quadratic)	$A + B \cdot \lambda + C \cdot \lambda^2$	$B + 2 \cdot C \cdot \lambda$
3rd order polynomial (cubic)	$A + B \cdot \lambda + C \cdot \lambda^2 + D \cdot \lambda^3$	$B + 2 \cdot C \cdot \lambda + 3 \cdot D \cdot \lambda^2$
4th order polynomial	$A + B \cdot \lambda + C \cdot \lambda^2 + D \cdot \lambda^3 + E \cdot \lambda^4$	$B + 2 \cdot C \cdot \lambda + 3 \cdot D \cdot \lambda^2 + 4 \cdot E \cdot \lambda^3$

Table A.2 — Slope equations

Fit type	Equation for dispersion slope
3-term Sellmeier	$2 \cdot B + 6 \cdot C \cdot \lambda^{-4}$
5-term Sellmeier	$2 \cdot B + 6 \cdot C \cdot \lambda^{-4} + 12 \cdot D \cdot \lambda^2 + 20 \cdot E \cdot \lambda^{-6}$
2nd order polynomial (quadratic)	$2 \cdot C$
3rd order polynomial (cubic)	$2 \cdot C + 6 \cdot D \cdot \lambda$
4th order polynomial	$2 \cdot C + 6 \cdot D \cdot \lambda + 12 \cdot E \cdot \lambda^2$

Table A.3 — Zero-dispersion wavelength and slope equations

Fit type	Zero-dispersion wavelength	Zero-dispersion slope
3-term Sellmeier	$(C/B)^{1/4}$	8B

Fit type	Zero-dispersion wavelength	Zero-dispersion slope
2nd order polynomial (quadratic)	–B/(2C)	2C

A.3. Fitting procedure

For robust numerical fitting, the natural abscissa (wavelengths) should be converted to values with a reduced range by a change of coordinates before completing the least squares regression. After the regression, the fitting parameters must be converted back to the original wavelength scale before completing any of the derivatives.

A suitable implementation of least squares regression should be chosen to solve the fitting problem. The method should be stable towards noise and other errors introduced during the measurement of the group delay or dispersion data. (See, e.g., [b-Press].) Depending on the source of the input data, equations for group delay or the derivative dispersion is used.

Care should be taken to include a sufficient number of points in the fitting. When the fitting order and the number of points become comparable, the fitting will not yield accurate results.

If the fit is made to group delay data, chromatic dispersion data can be calculated from the dispersion equations in Table A.1, using the coefficients found from the fit. Extrapolation to wavelengths outside the fitting region should be used carefully, as the fits might have unphysical behaviour at points outside the region.

The dispersion slope can be calculated from the equations in Table A.2, using the coefficients found from the fit.

Appendix I

Methods of cut-off wavelength interpolation

(This appendix does not form an integral part of this Recommendation.)

This appendix presents methods of determining the coefficients, A_t and B_t found in Equation (6-11). Limited negative error method and least square method are described in clauses clause I.1 and clause I.2, respectively. Clause I.3 provides an example of the cut-off wavelength interpolation method.

I.1. Limited negative error method

The algorithm is derived from the observation that the transition structures (humps) consist of data points with a positive deviation from the expected ideal curve. The interpolation procedure is based on a theoretical model of the LP_{11} transition region and a method of fitting the data to the model. The procedure has six steps.

The first two steps define the LP_{01} region, or upper wavelength region. The second two steps define the transition region, where LP_{11} attenuation begins to increase. The fifth step characterizes this region according to a theoretical model. The last step computes the cut-off wavelength, λ_c, from the characterization parameters.

Step 1 – Define the upper wavelength region

Lower wavelength of the region

For multimode reference:

Find the maximum slope wavelength, the wavelength at which the first difference a(λ) – a(λ+0.01), is largest. For wavelengths greater than the maximum slope wavelength, the lower wavelength of the region is the wavelength at which the attenuation is minimum.

For bend reference, the following simulates the procedure for multimode reference:

Find the maximum attenuation wavelength. For wavelengths greater than the maximum attenuation wavelength, the lower wavelength of the region is the wavelength at which the following function is minimum:

$$a(\lambda)-8+8\lambda(\lambda \text{ in } \mu m)$$

Upper wavelength of the region

Lower wavelength of region plus 0.15 µm.

Step 2 – Characterize the attenuation curve, a(λ), of the upper wavelength region as a linear equation in wavelength, λ

$$a(\lambda)\cong A_u+B_u\lambda \qquad \text{(I-1)}$$

The following approaches are suggested:

Bend reference method:

Set $B_u = 0$

Set A_u = median of attenuation values in the upper wavelength region.

Multimode reference method:

Find A_u and B_u so that the sum of the absolute values of error in the upper wavelength region is minimum and so that all errors are non-negative. Find the median of the errors in the upper wavelength region and add to A_u.

Determine the most negative error of the upper wavelength region, E:

$$E = \min\left[a(\lambda) - A_u - B_u\lambda\right] \tag{I-2}$$

Step 3 – Find the upper wavelength of the transition region

Starting at the upper wavelength of the upper wavelength region, from Step 1, determine the maximum wavelength at which the attenuation is 0.1 dB greater than the line found in Step 2. Set the upper wavelength of the transition region to this value plus 10 nm.

Step 4 – Find the lower wavelength of the transition region

There are various methods to determine this wavelength. The following are examples:

Let:

$$\Delta a(\lambda) = a(\lambda) - A_u - B_u(\lambda) \tag{I-3}$$

a) Starting with the upper wavelength of the transition region, from Step 3, find the wavelength at which $\Delta a(\lambda)$ has a local maximum and so the difference between this maximum and the next local minimum (at larger λ) is maximum.

b) The largest wavelength, below the upper wavelength of the transition region, so that: $\Delta a(\lambda)$ is greater than 2 dB; and
   1) there is a local maximum for $\Delta a(\lambda)$; or
   2) there is a local maximum for $\Delta a(\lambda) - \Delta a(\lambda + 0.01)$.

Step 5 – Characterize the transition zone with the model and constraints on errors

The model is a linear regression of a transformation. Constraints on errors control negative regression errors so that the inverse transform of the fitted line will not produce negative attenuation errors less than E, from Step 2. Fitting the data with constraints on errors may be done with simplex linear programming methods.

Find A_t and B_t, from Equation (6-11), so that the sum of the absolute values of error is minimized and so that no error is less than $-v(\lambda)$, with $v(\lambda)$ given as a function of E, from Step 2:

$$w(\lambda) = 10^{\frac{\Delta a(\lambda) - E}{10}} \tag{I-4}$$

$$z(\lambda) = 10\log\left[-\frac{10}{A}\log\left(\frac{w(\lambda)-1}{\rho}\right)\right] \tag{I-5}$$

$$v(\lambda) = Y(\lambda) - z(\lambda) \tag{I-6}$$

Step 6 – Evaluate the slope of the transition and compute the cut-off wavelength, λ_c

If B_t is greater than some small negative values, e.g., –1 to –0.1, reduce the upper wavelength of the transition region by 10 nm and repeat Step 5.

Otherwise, compute λ_c:

$$\lambda_c = -\frac{A_t}{B_t} \tag{I-7}$$

I.2. Least squares method

This algorithm is based on the assumption that the structure sometimes seen in the transition region is caused by an interference effect around the position of the ideal curve.

The mathematical model is the same as that used in the limited negative error method.

Step 1 – As limited negative error method.

Step 2 – As limited negative error method. E in Equation (I-2) is not required.

Step 3 – As limited negative error method.

Step 4 – As limited negative error method.

Step 5 – Characterize the transition zone.

The model is a least squares best fit of a transformation.

Find A_t and B_t from Equation (6-11), so that the sum of the squares of the errors is minimized, using Equation (6-7), Equation (6-8), Equation (6-9) and:

$$W(\lambda) = 10^{\Delta a(\lambda)/10} \tag{I-8}$$

Step 6 – As limited negative error method.

I.3. Example

Figure I.1 shows an example of the cut-off plot for several fibre samples. In the absence of spurious humps or excessive noise in the upper-wavelength region, accurate values for cut-off wavelength can be determined without an interpolation method (Sample 1, 2, 5 in Figure I.1). On the contrary, the interpolation method will be helpful to determine the cut-off wavelength and improve the precision (Sample 3, 4 in Figure I.1).

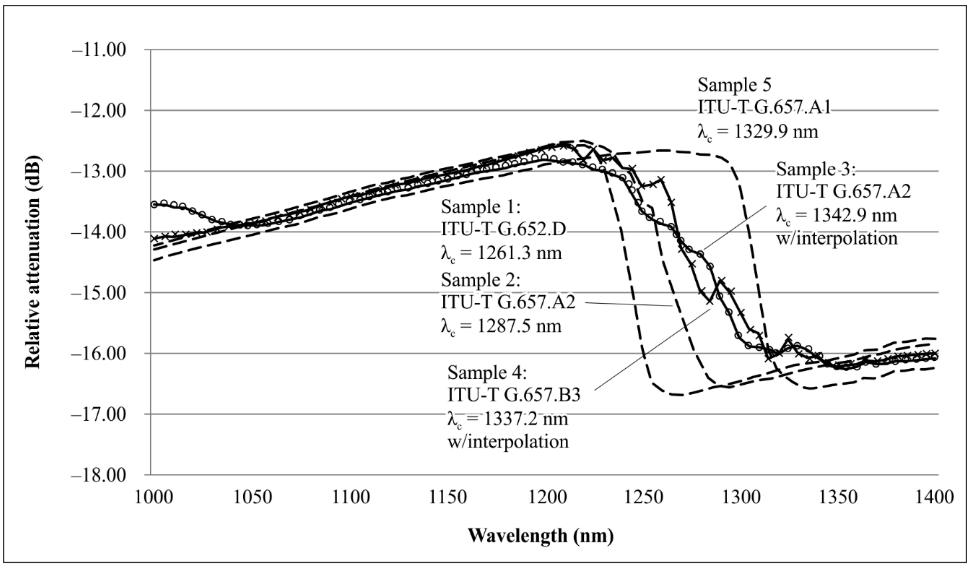


Figure I.1 — Cut-off wavelength interpolation for some fibre samples

Appendix II

Test method for measuring longitudinal uniformity of chromatic dispersion based on the backscattering technique

(This appendix does not form an integral part of this Recommendation.)

II.1. General

A test method is described by which to determine the longitudinal uniformity of the chromatic dispersion of a single-mode optical fibre based on bidirectional backscattering measurements. This technique can evaluate the uniformity of the waveguide and material dispersion individually. Moreover, this technique can be used to measure the mode field diameter. Procedures for the calibration of backscattering equipment are provided in [IEC 61746-1].

II.2. Test apparatus

II.2.1. General considerations (as in clause 6.4.2.2.1)

An example of the apparatus is shown in Figure II.1.

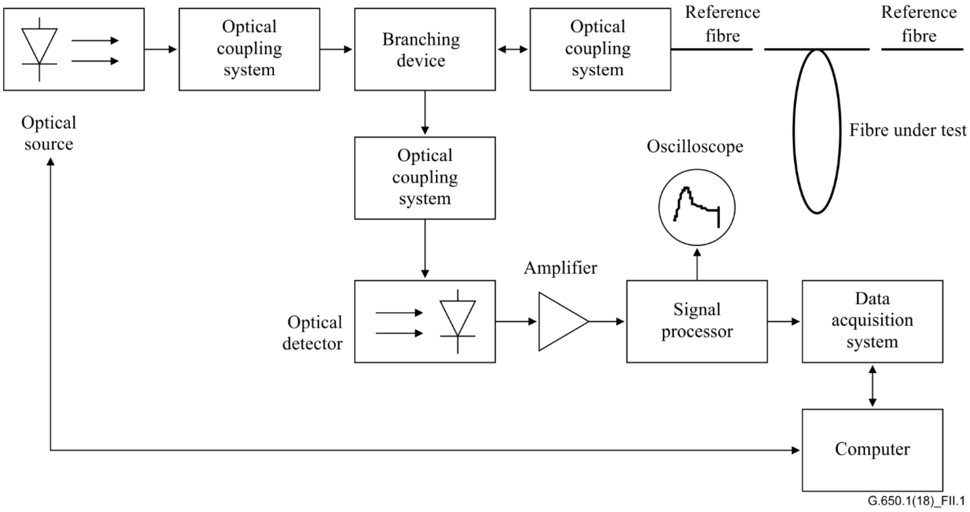


Figure II.1 — Schematic of apparatus for chromatic dispersion uniformity measurement

II.2.2. Optical source (as in clause 6.4.2.2.2)

II.2.3. Optical coupling system (as in clause 6.4.2.2.3)

II.2.4. Branching device (as in clause 6.4.2.2.4)

II.2.5. Optical detector (as in clause 6.4.2.2.5)

II.2.6. Amplifier (as in clause 6.4.2.2.6)

II.2.7. Signal processor (as in clause 6.4.2.2.7)

II.2.8. Cladding mode stripper (as in clause 6.4.2.2.8)

II.2.9. Reference fibre

The refractive index profile of the reference fibre shall be similar to that of the test fibre and its length is restricted to maintain a good longitudinal uniformity, but it shall be longer than the input dead-zone of the backscattering measurements. In addition, the mode field diameter of the reference fibre shall be measured as a function of wavelength. This reference fibre can be used to estimate the absolute value of the mode field diameter and relative index difference from the backscattering measurements.

II.3. Measurement procedure

a) Connect reference fibres to both ends of the test fibre.

b) Align the fibre under test with the optical coupling system.

c) As b) in clause 6.4.2.3.

d) As c) in clause 6.4.2.3.

e) Obtain the bidirectional backscattering imperfection loss curve using the two measured and recorded unidirectional backscattering loss curves, according to the procedure outlined in the following:

Let $S_1(x)$ and $S_2(z)$ be functions describing the two unidirectional backscattering loss curves expressed in dB, with x and z being the distances from the fibre ends nearest the respective launch sites and $L = x + z$. The bidirectional backscattering imperfection loss curve is given by:

$$I(x, z) = \frac{S_1(x, \lambda) + S_2(L - x, \lambda)}{2} \quad \text{(II-1)}$$

f) Obtain the imperfection loss normalized by that at position x_0 in the reference fibre according to the procedure outlined in the following:

$$I_n(x, \lambda) = I(x, \lambda) - I(x_0, \lambda)$$

$$= 20\log\left\{\frac{W(x_0, \lambda)}{W(x, \lambda)}\right\} + 10\log\left[\left\{\frac{1+0.62\,\Delta(x)}{1+0.62\,\Delta(x_0)}\right\}\left\{\frac{50-\Delta(x)}{50-\Delta(x_0)}\right\}\right]$$

$$= 20\log\left\{\frac{W(x_0, \lambda)}{W(x, \lambda)}\right\} + k \quad \text{(II-2)}$$

where coefficient k is defined as:

$$k = 10\log\left[\left\{\frac{1+0.62\,\Delta(x)}{1+0.62\,\Delta(x_0)}\right\}\left\{\frac{50-\Delta(x)}{50-\Delta(x_0)}\right\}\right] \quad \text{(II-3)}$$

g) Obtain the mode field diameter distribution $2\,W(x, \lambda)$ according to the procedure outlined in the following:

Let the mode field diameter at position x_0 in the reference fibre be $2\,W(x_0, \lambda)$. The mode field diameter distribution is given by:

$$2W(x, \lambda) = 2W(x_0, \lambda) \cdot 10^{\frac{-I_n(x,\lambda)+k}{20}} \quad \text{(II-4)}$$

If the reference and test fibres have the same index profile and relative index difference, let coefficient $k = 0$.

If the relative index difference in the test fibre is not the same as that in the reference fibre, determine coefficient k by using Equation (II-3) and the mode field diameter value at x in the test fibre which is evaluated in advance.

If the adjustment factors f and g, which are determined as described in c) in clause clause 6.1.4.3.2, are given, the mode field diameter distribution is given by:

$$2W(x, \lambda) = 2W(x_0, \lambda) \cdot 10^{\frac{-g \cdot I_n(x,\lambda)+f}{20}} \quad \text{(II-5)}$$

If the relative index difference in the test fibre is unknown, the mode field diameter value at x in the test fibre is obtained with Equation (II-6) considering the second position x_1 in the reference fibre.

$$2W(x, \lambda) = 2W(x_0, \lambda) \cdot \left[\frac{2W(x_1, \lambda)}{2W(x_0, \lambda)}\right]^{\frac{I(x,\lambda)-I(x_0,\lambda)}{I(x_1,\lambda)-I(x_0,\lambda)}} \quad \text{(II-6)}$$

h) Repeat the above procedures for two or more different wavelengths.

i) Obtain the coefficients g_0, g_1, and g_2 which satisfy Equation (II-7) using the above mode field radii $W(x, \lambda)$:

$$W(x,\lambda) = g_0(x) + g_1(x)\lambda^{1.5} + g_2(x)\lambda^6 \quad \text{(II-7)}$$

(three or more wavelengths)
or:

$$W(x,\lambda) = g_0(x) + g_1(x)\lambda^{1.5} \quad \text{(II-8)}$$

(two or more wavelengths)
This expression may be evaluated by a least squares fit of the data $W(x, \lambda_i)$ ($i = 1, \ldots, n$).

j) Obtain the waveguide dispersion distribution $D_w(x, l)$ in ps/(nm × km) outlined in the following:

$$D_w(x,\lambda) = \frac{\lambda}{2\pi^2 cnW(x,\lambda)^2}\left\{1 - \frac{2\lambda}{W(x,\lambda)}\left(\frac{3}{2}g_1(x)\lambda^{0.5} + 6g_2(x)\lambda^5\right)\right\} \quad \text{(II-9)}$$

(three or more wavelengths)
or:

$$D_w(x,\lambda) = \frac{\lambda}{2\pi^2 cnW(x,\lambda)^2}\left\{1 - \frac{3g_1(x)\lambda^{1.5}}{W(x,\lambda)}\right\} \quad \text{(II-10)}$$

(two or more wavelengths)
where c and n show the light velocity in m/s and the maximum refractive index of the core, respectively.

k) Obtain the relative index difference distribution $\Delta(x)$ in % according to the procedure outlined in the following:
If the reference and test fibres have the same index profile, obtain the coefficients c_0, c_1 and c_2 at the reference fibre which satisfy the following equation using mode field diameter 2 $W(x_0$, l), core diameter $2a(x_0)$ and cut-off wavelength $\lambda_c(x_0)$:

$$\frac{W(x_0,\lambda)}{a(x_0)} = c_0 + c_1\left\{\frac{\lambda}{\lambda_c(x_0)}\right\}^{1.5} + c_2\left\{\frac{\lambda}{\lambda_c(x_0)}\right\}^{6} \tag{II-11}$$

Calculate the characteristic of the ratio R_W of mode field diameters of two wavelengths (λ~1 ~and λ_2) as a function of the cut-off wavelength λ_c using the above coefficients c_0, c_1 and c_2.

$$R_W = \frac{2W(\lambda_1)}{2W(\lambda_2)} = \frac{c_0 + c_1\left(\frac{\lambda_1}{\lambda_c}\right)^{1.5} + c_2\left(\frac{\lambda_1}{\lambda_c}\right)^{6}}{c_0 + c_1\left(\frac{\lambda_2}{\lambda_c}\right)^{1.5} + c_2\left(\frac{\lambda_2}{\lambda_c}\right)^{6}} \tag{II-12}$$

Determine the approximate function between the ratio R_W of mode field diameters at two wavelengths and cut-off wavelength λ_c.
Obtain the cut-off wavelength distribution $\lambda_c(x)$ by applying the above approximate function to the ratio of the measured mode field diameter distributions.
Obtain the core diameter distribution $2a(x)$ substituting the mode field diameter distribution 2 $W(x)$ and the cut-off wavelength distribution $\lambda_c(x)$ into Equation (II-11).
Obtain the relative index difference distribution $D(x)$ in % using Equation (II-13):

$$\Delta(x) = \left\{\frac{a(x_0)}{a(x)}\right\}^2 \left\{\frac{\lambda_c(x)}{\lambda_c(x_0)}\right\}^2 \Delta(x_0) \tag{II-13}$$

Alternatively, relative index difference $\Delta(x)$ in % is obtained with Equation (II-14) using the relative index difference at position x_0 in the reference fibre $\Delta(x_0)$.

$$\Delta(x) = \frac{1}{0.62}\left[\{1 + 0.62\,\Delta(x_0)\}\cdot 10^{\frac{I_{II}(x,\lambda) - 20\log\left\{\frac{2W(x_0,\lambda)}{2W(x,\lambda)}\right\}}{10}} - 1\right] \tag{II-14}$$

l) Obtain the material dispersion distribution $D_m(x, \lambda)$ in ps/(nm × km) using the above relative index difference distribution $\Delta(x)$.
Here, the approximate equation of the material dispersion can be obtained as a function of wavelength and relative index difference.
The material dispersion $D_m(\lambda)$ can be estimated by using Equation (II-15) and Equation (II-16):

$$D_m(\lambda) = -\frac{\lambda}{c}\frac{d^2 n(\lambda)}{d\lambda^2} \quad \text{(II-15)}$$

$$n^2(\lambda) - 1 = \sum_{i=1}^{k} \frac{B_i \lambda^2}{\lambda^2 - A_i^2} \quad \text{(II-16)}$$

where A_i and B_i show the Sellmeier coefficients and both coefficients A_i and B_i as a function of dopant content corresponding to the relative-index difference D were given in [b-Kobayashi] and [b-Fleming].
Calculate an estimated function $D_m(\lambda)$ of material dispersion against the relative-index difference D by using Equation (II-15) and Equation (II-16).
The material dispersion against the relative-index difference D is obtained as follows:

$$D_m(\lambda) = m_1(\lambda) + h \cdot \Delta \cdot m_2(\lambda) \quad \text{(II-17)}$$

where h shows the constant.
Obtain the chromatic dispersion distribution $D(x,\lambda)$ in ps/(nm × km) outlined in the following:

$$D(x, \lambda) = D_m(x, \lambda) + D_w(x, \lambda) \quad \text{(II-18)}$$

II.4. Presentation of the results

The following details shall be presented:

a) test set-up arrangement;
b) kind of signal processing used;
c) pulse width;
d) test wavelengths;
e) mode field diameter distribution in µm;
f) chromatic dispersion distribution in ps/(nm × km).

Appendix III

Example of a matrix model

(This appendix does not form an integral part of this Recommendation.)

The following is an example of an m × n = 38 × 3 matrix, as described in clause 6.4.4.3, for [ITU-T G.652] fibres. Please note it is given for illustrative purposes only. If the spectral attenuation is to be estimated over the range of 1240 nm to 1600 nm (in steps of 10 nm) using 1310 nm, 1380 nm and 1550 nm as predictor wavelengths, an example of matrix elements which has been shown to be applicable [b-Hanson] for some [ITU-T G.652] fibres follows:

Output wavelength (μm)	Predictive wavelengths		
	1310 nm	**1380 nm**	**1550 nm**
1.23	1.46027	–0.04235	–0.20771
1.24	1.35288	–0.01493	–0.13289
1.25	1.31704	–0.00412	–0.14768
1.26	1.26613	–0.00997	–0.13715
1.27	1.20167	–0.00843	–0.10635
1.28	1.14970	–0.01281	–0.06363
1.29	1.11290	–0.01059	–0.06245
1.30	1.03600	–0.00711	0.00711
1.31	0.96276	0.00342	0.05412
1.32	0.90437	0.01435	0.08572
1.33	0.86168	0.02098	0.11776
1.34	0.83194	0.05500	0.05849
1.35	0.73415	0.08336	0.14196
1.36	0.83266	0.11032	–0.10694
1.37	0.69137	0.22596	–0.05961
1.38	0.01006	0.99798	–0.01126
1.39	–0.25502	0.94764	0.48887
1.40	0.00227	0.58463	0.51813
1.41	0.25780	0.33834	0.40811
1.42	0.29085	0.20419	0.49620
1.43	0.29329	0.13569	0.54995
1.44	0.33133	0.09266	0.51936
1.45	0.31608	0.06343	0.55905
1.46	0.24183	0.04483	0.68361
1.47	0.29207	0.03019	0.59222
1.48	0.19214	0.02196	0.75669
1.49	0.18650	0.01132	0.76122
1.50	0.21242	0.00541	0.70722
1.51	0.16884	0.00648	0.75347
1.52	0.11484	–0.00091	0.84972
1.53	0.09334	0.00419	0.85304
1.54	0.07231	–0.00021	0.88512
1.55	0.03111	–0.00115	0.94957
1.56	0.07054	–0.00321	0.87414
1.57	–0.03723	–0.01127	1.08140
1.58	–0.02543	0.00556	1.01041
1.59	–0.01370	0.00457	0.99389
1.60	–0.06916	–0.00107	1.11623

Appendix IV

Test methods for measuring coherent MPI in short optical fibre cables (jumpers)

(This appendix does not form an integral part of this Recommendation.)

The measurement of coherent multipath interference (MPI) is performed to ensure low noise contribution from a short (typically < 10 m) cabled optical fibre. This test is particularly relevant to [ITU-T G.657] fibres, as they present a wide variety of high-order mode (HOM) transmission characteristics and tend to tightly bind these modes to the fibre core (mode stripping is difficult). MPI values are measured as a function of wavelength, with particular attention to the shortest wavelengths to be used over the cable. The result will be a function of both the length of the cable sample and the splice (connector) loss at the cable ends. Hence these parameters should be quantified and shared by the manufacturer. A further variable is the cable geometrical layout. A straight cable layout will generally give the highest MPI though "resonance wavelengths" may appear where the HOM is strongly damped, and the MPI is very low. More realistic geometries are preferred and are obtained by using controlled bending of the cable.

There are three methods for measuring MPI. The first, the "Narrowband ECL/PM method", uses an external cavity laser (ECL) and a power meter (PM) and is quite accurate but may be time consuming and limited in wavelength range. The second, the "Wideband LED/OSA method", uses a wideband source (such as an edge emitting light emitting diode, EELED) and an optical spectrum analyser (OSA). This method typically has a higher noise floor but enables MPI measurements over the entire transmission band of the fibre. The third method uses a fixed wavelength light source, such as in an actual transmitter, and involves varying the length of the jumper by stretching. It is termed the "Fibre stretching" or "FS" method. This method has the advantages of:

1) low cost light sources;
2) ability to find MPI using actual transceivers in a system test arrangement; and
3) avoidance of extraneous wavelength dependencies in the test set-up.

Disadvantages include a more complicated set-up and the inability to measure fibres in configurations other than straight, under tension.

IV.1. First test method: The narrowband ECL/PM technique

IV.1.1. General

The narrowband ECL/PM technique monitors transmitted optical power through the jumper as a function of wavelength. The interference phenomenon between the fundamental, LP_{01}, and HOM is measured by capturing the maximum and minimum transmitted power over a range of wavelengths. Polarization variation of the input is used to ensure true power extremes are found.

IV.1.2. Test apparatus

A schematic of the apparatus required for the first test method is shown in Figure IV.1.

IV.1.2.1. Optical source

A tuneable external cavity laser (ECL) is used with recommended characteristics: line width < 200 kHz, power > –4 dBm at the shortest wavelengths of interest (usually 1260 nm) and wide tuning range (~100 nm). The stability of the power should be < 0.01 dB over the testing time and should vary < 0.05 dB over the wavelength range required to sample the free spectral range (FSR) of the jumper interference pattern (this is typically ~2 nm). The laser RIN should be less than −145 dBm/Hz over the 10 MHz-500 MHz range. It is useful to measure the MPI of the ECL in isolation and values typically are < –55 dB. Output should be taken through a standard single-mode fibre ([ITU-T G.652] type) with an angled connector.

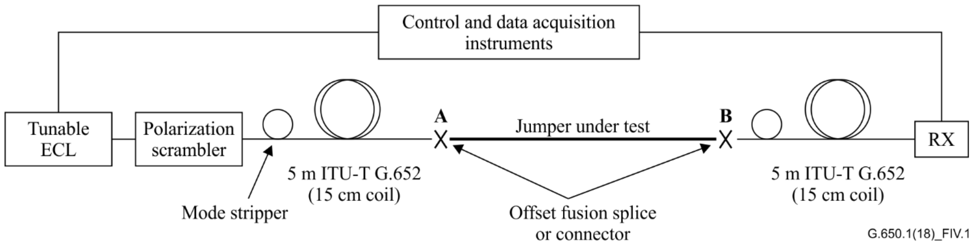


Figure IV.1 — Schematic of set-up for narrowband ECL/PM method.Here the "RX" receiver consists of a power meter or a photodetector/oscilloscope pair

IV.1.2.2. Polarization scrambler

Since the coupling at the connection points will be polarization dependent, power measurements must be made at many random polarizations of the incoming light. The polarization may be changed by use of a polarization controller (manual or electronic) or a scrambler. In the case of a controller, at least 100 randomized polarization states should be used for each wavelength measured (therefore the manual controller is not recommended). The use of the scrambler requires knowledge of the scrambling speed (degree/s change on the Poincaré sphere, or highest frequency component in the scrambling instrument). The power measurement must be made on a time scale that is short compared to the time for the polarization to change substantially. Power meters usually require ~0.1– 20ms to obtain a reading. Thus scrambling frequencies should be below the range 1–0.005 kHz, depending on the averaging time chosen for the power meter. If the photodetector/OSA receiver is used (see clause IV.1.2.4 below) then the scrambling speed is virtually unlimited. The polarization scrambler should have angled connections. It is useful to test the combined ECL – scrambler combination for MPI. Typical results are < –50 dB. Verify that randomly distributed polarization states on the Poincaré sphere are obtained.

IV.1.2.3. Mode stripping loop

The single-mode fibre in the launch line should be looped to the appropriate dimension to eliminate all but the fundamental LP_{01} mode propagation. An alternative is to use a long (several hundred metres) piece of [ITU-T G.652] fibre to sufficiently attenuate the HOM.

IV.1.2.4. Optical receiver

The light should be received by a power meter or a photodetector/oscilloscope combination. The power meter averaging time should be adjusted so that power measurements are made rapidly compared to the time over which the polarization scrambler changes the polarization significantly. Linearity of the power meter at the power levels used in the test should be ensured. The power meter response should be corrected for the different wavelengths used in the test. Built-in software may allow the power meter to run in MIN-MAX mode or LOGGING mode to get power statistics. Data is collected at each wavelength until > 100 measured power values have been captured.

The photodetector/oscilloscope combination allows very high scrambling rates to be used (thereby shortening the testing time). Operate at high optical power to minimize receiver noise (but verify linearity of the detector at these power levels). Use a vertical offset on the oscilloscope trace and expand the vertical scale to maximize signal capture. Do not average. Set the acquisition sample rate according to a polarization scrambling speed and maximize the number of samples (record length). Set the time base to either capture all data in a single trigger and identify maximum and minimum voltages or run multiple triggers with a fast time base and collect voltage extrema over a sequence of triggers. The oscilloscope data acquisition should be triggered in synchronism with the ECL wavelength steps.

IV.1.3. Measurements procedure

IV.1.3.1. Preparation of the fibre under test

If the short cable (fibre) to be tested has connectors, make sure proper cleaning procedures are followed. Choose a cable length to be tested and connectorize the ends or prepare the ends for fusion splice.

IV.1.3.2. Baseline measurement

This step identifies the lowest MPI the test set-up is capable of measuring. In addition, the average transmitted power obtained here is useful in removing the light source power variation with wavelength as prescribed in clause IV.1.3.5.

Before including the test cable in the measurement set-up, measure a baseline response by connecting the polarization scrambler and RX in Figure IV.1 with either a 10 m long [ITU-T G.652] fibre or two connectorized 5 m [ITU-T G.652] fibres. Angled connectors should be used for both ends of the [ITU-T G.652] fibre. Sweep the wavelength (over a range of roughly ±3 nm) in steps small enough to resolve the interference fringes expected in the test cable (iteration might be required, or use a small step such as 0.02 nm). At each wavelength capture the minimum, maximum and average power for > 100 randomized polarization values. Use a wide enough wavelength scan to capture the free spectral range (FSR) of the jumper interference pattern. Since the FSR is not known before the jumper is measured, the baseline measurement might need to be repeated after a jumper measurement has been performed.

IV.1.3.3. Insert short-cabled fibre

Either disconnect the two 5 m [ITU-T G.652] fibres or cut the [ITU-T G.652] fibre at its centre and insert the test cable into the set-up (between points A and B in Figure IV.1), and characterize splice/ connector losses at each end. Intentional offset fusion splices are a convenient way to obtain a desired connection loss. An alternative is to use offset connectors. When the MFD values of ITU-TG.652 fibre and test fibre are 9.0±0.5 µm at 1310 nm, an offset of 1-2 µm corresponds to a connection loss of 0.5-1 dB (this loss should be directly measured). The coupling ratio of LP_{01} power in the 5m [ITU-T G.652] fibre lead to LP_{01} power in the test cable is desired for both connection points. It may be necessary to use mode filters and trial and error to eliminate the higher order modes (see the following note for more details). The geometrical layout of the test cable may be substantially straight, as this is the configuration which will generally give worst case MPI results. Other, more preferable, configurations can be tested as well, which involve multiple small radius cable bends.

NOTE – The meaning of the MPI value obtained from this measurement is unclear without accurate knowledge of the LP_{01} loss through each of the connection points. Stripping of the high-order mode is required to determine this loss. Some additional comments are made here on mode stripping in [ITU-T G.657] fibres. Some [ITU-T G.657].A fibres may be mode stripped by using a suitably small fibre loop (the loop should not be so small that it attenuates the LP_{01} mode). If this is the case for the fibre under test, the first connection is made while monitoring the power through the jumper with a mode stripping loop present. When the first connection is satisfactory, the second connection is made, again with mode stripping loops present and power through the 5 m [ITU-T G.652] fibre jumper is monitored until the total loss (through both splices) is satisfactory.

Some [ITU-T G.657].A fibres and all [ITU-T G.657].B fibres cannot be mode stripped with fibre loops. However, these fibres generally do have a substantial HOM loss with fibre length (even when straight). Lengths required to strip out the HOM may be several hundred metres for some fibre types. In this case the first offset connection is made between the 5 m [ITU-T G.652] fibre and a spool of the desired jumper fibre. Accounting for the LP_{01} loss through the spool (this may be measured separately using an aligned splice to the [ITU-T G.652] launch fibre) the offset connection is adjusted until the desired LP_{01} loss is obtained. The spooled test fibre is now cut back to the desired jumper length and connectorized or fusion spliced to the output 5 m [ITU-T G.652] fibre. Loss through this second connection point is found by monitoring power at the RX and comparing with LP_{01} input power minus the first connection LP_{01} loss.

In either case, LP_{01} loss data should be taken over the FSR (~ ±3 nm) of the jumper interference pattern. The average over this wavelength range is the connection loss. For consistency, it is important to equalize the splice loss at each end of the test cable. This is because, for a fixed total loss in the splices, maximum MPI is found when the individual splice losses are equal.

IV.1.3.4. Short-cabled fibre measurement

The measurement procedure of clause IV.1.3.2 is followed. With the jumper under test included, ensure that the wavelength scan range is sufficient to encompass several cycles of the roughly sinusoidal variation in transmitted power of the FSR. In addition, ensure that the wavelength step is sufficiently small to resolve the spectral intensity pattern.

IV.1.3.5. Calculations

Though not mandatory, it is informative to first subtract the baseline average power from the maximum and minimum power measured through the test cable. This corrects for the power variation with wavelength of the light source. To compute the MPI, the data (corrected maximum and minimum transmitted power versus wavelength) is processed through a moving window of width ≥ FSR. For each position of the window (denoted by its central wavelength), the maximum and minimum power are found and used in Equation (IV-1) to find the MPI.

$$MPI(dB) = 20\log\left[\frac{10^{\mathrm{PR}/20}-1}{10^{\mathrm{PR}/20}+1}\right] \qquad \text{(IV-1)}$$

where PR is the difference between the maximum and minimum power levels detected (in dB). Note that if the photodetector/oscilloscope method is used, the output data is an electrical voltage, not an optical power. Due to the linearity of the photodetector, Equation (IV-1) can still be used with a voltage difference when voltages have been converted to dB (10 log V). Dark current corrections should be made prior to this conversion. Verify that the MPI, computed directly from the baseline data, is suitably low.

IV.1.3.6. Presentation of the results

The following details shall be presented:

a) test set-up arrangement;
b) optical source characteristics;
c) polarization scrambling rate;
d) fibre identification (cabled or uncabled), length, insertion loss and splice loss;
e) methodology for measuring insertion/splice loss;
f) geometrical layout of test cable;
g) receiver characteristics (including signal acquisition time);
h) table of MPI versus wavelength;
i) after data is taken for a number of fibres of a given design, a mapping between the cut-off wavelength and MPI noise may be compiled.

IV.2. Second test method: The wideband LED/OSA technique

IV.2.1. General

The wideband LED/OSA technique monitors transmitted optical power through the jumper under test as a function of wavelength. The interference phenomenon between the fundamental, LP_{01}, and HOM is measured by capturing the maximum and minimum transmitted power over a range of wavelengths. Polarization variation of the input is used to ensure true power extremes are found.

IV.2.2. Test apparatus

A schematic of the apparatus required for the second test method is shown in Figure IV.2.

IV.2.2.1. Optical source

A wideband light source (typically LED-based) with peak power density > –40 dBm/nm and stability < ±0.03 dB/15 minutes with output in the wavelength range of interest (usually 1260-1625 nm). Note that the stability of this source will not be as good as the ECL used in the first test method. This limits the lowest MPI which can be measured. It is useful to measure the MPI of the wideband source in isolation and values typically are < –40 dB across the full spectral band. Output should be taken through [ITU-T G.652] fibre. Angled connectors should be used when available.

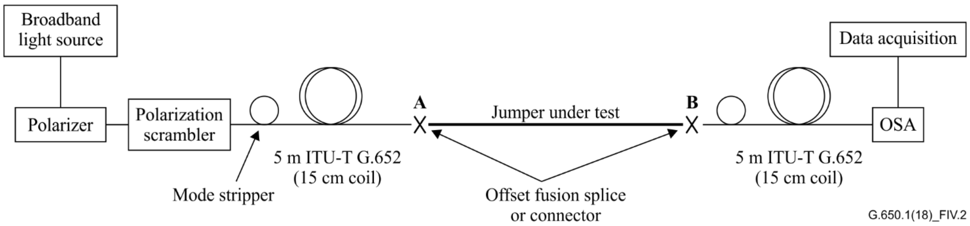


Figure IV.2 — Schematic of set-up for the wideband LED/OSA method. The polarizer is not necessary if the broadband light source has an internal polarizer

IV.2.2.2. Polarization scrambler

Since the coupling at the connection points will be polarization dependent, OSA power density measurements must be made at many random polarizations of the incoming light. The polarization may be changed by use of a polarization controller (manual or electronic) or a scrambler. In the case of a controller, at least 100 randomized polarization states should be used for each wavelength measured (therefore a manual controller is not recommended). The use of the scrambler requires knowledge of the scrambling speed (degree/sec change on the Poincaré sphere, or highest frequency component in the scrambling instrument). The OSA power density measurement at each wavelength must be made on a time scale which is short compared to the time for the polarization to change substantially. Adjustment of the number of wavelengths tested, the sweep speed and the sensitivity allows the user to vary the acquisition time of the OSA to match the speed of the polarization scrambler. Note that only slow scrambling speeds are possible. The polarization scrambler should have angled connections. It is useful to test the LED – scrambler combination for MPI. Verify that randomly distributed polarization states on the Poincaré sphere are obtained.

IV.2.2.3. Mode stripping loop

See clause IV.1.2.3.

IV.2.2.4. Optical receiver

The OSA should be configured with the correct number of wavelength points and the sweep time so that the residence time at each wavelength is much shorter (~10 times) than the inverse of the polarization scrambling speed. This prevents polarization averaging during OSA measurement at each wavelength. Choose the vertical scale to maximize the signal. Measurements are taken using the MAXIMUM and MINIMUM power density functions on the OSA (if available). Resolution bandwidth should be 0.1 nm or less and the number of wavelength points should be sufficient to resolve the interference fringes over the FSR.

IV.2.3. Measurements procedure

IV.2.3.1. Preparation of the fibre under test

See clause IV.1.3.1.

IV.2.3.2. Baseline measurement

Before including the test cable in the measurement set-up, measure a baseline response by connecting the polarization scrambler and OSA in Figure IV.2 with a 10 m long [ITU-T G.652] fibre. With the OSA configured with the correct number of wavelengths, sweep speed, resolution bandwidth and vertical scale, apply averaging and measure the baseline response. Maxima and minima can also be measured if baseline MPI data is desired. Save the averaged trace for use later in removing the spectral dependency of the power output from the LED source.

IV.2.3.3. Insert short-cabled fibre

See clause IV.1.3.3.

IV.2.3.4. Short-cabled fibre measurement

Procedure if OSA has MAX power and MIN power trace capabilities: Put the OSA into MAX trace mode. Allow > 100 sweeps to get the highest signal at each wavelength with respect to input polarization. Save this trace and perform the same test with the MIN trace mode (some OSA models can perform these acquisitions simultaneously). Subtract the baseline trace found in clause IV.2.3.2 from the MAX trace result and from the MIN trace result. Output the resulting two traces.

Procedure if the OSA does not perform MAX power and MIN power data manipulation internally: Take > 100 sweeps and output the data from each one to a control computer. Use the computer to sort out the maximum and minimum for each wavelength. The baseline can either be subtracted on the OSA or during data sorting on the computer.

IV.2.3.5. Calculations

See clause IV.1.3.5.

IV.2.3.6. Presentation of the results

See clause IV.1.3.6.

IV.3. Third test method: The fibre stretching technique

IV.3.1. General

The fibre stretching technique utilizes the fact that the transmitted power, with interference between the LP_{01} mode and an HOM in the jumper, changes periodically with the optical phase difference through the jumper. This optical phase difference is dependent on wavelength (which was exploited in the other two techniques) but is also proportional to the jumper length. The length is most easily varied by stretching the fibre. In this case the maximum and minimum transmitted power is measured as fibre length is varied. Polarization variation of the input is used to ensure true power extremes are found. For typical fibres with a 2 nm FSR, the required length variation is of the order of 2-4 mm; for a fibre span of 2 metres this corresponds to a strain of $\sim 10^{-3}$, substantially below proof test levels. Higher strains may be required for fibres with a larger FSR. This method may be less easily applied in cases where the jumper is buffered and/or jacketed.

IV.3.2. Test apparatus

A schematic of the apparatus required for the third test method is shown in Figure IV.3. The source can be either a tuneable laser or a transceiver. Polarization changes are made by the polarization scrambler. Angled connectors are used throughout to minimize reflections. The upstream fusion splice is attached to a fixed stage, while the other fusion splice is attached to a movable translation stage.

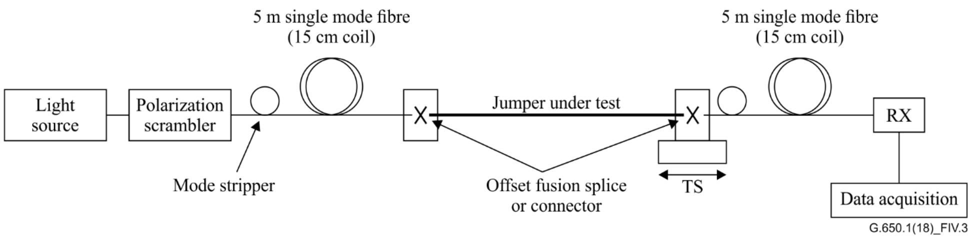


Figure IV.3 — Schematic of set-up for the fibre stretching method. "TS" is a translation stage. Here the "RX" receiver consists of a power meter or a photodetector/oscilloscope pair

IV.3.2.1. Optical source

If a tuneable laser is used, the laser performance should conform to the specifications given in clause IV.1.2.1. Alternatively, an optical transceiver may be used. In either case, ensure that wavelength and power output are stable over the several minutes required for performing the test. If an optical transceiver can be chosen which is comparable to that used in the actual deployed system, the MPI results are particularly relevant.

If a transceiver (e.g., a DFB one) with optical properties equivalent to those of the tuneable laser described in clause IV.1.2.1 is employed, the results will be substantially source-independent; otherwise (e.g., if a Fabry-Perot transceiver is used) the results may depend on the transceiver properties.

IV.3.2.2. Measurement settings

IV.3.2.2.1. Polarization scrambler

To ensure that worst-case conditions are achieved, transmitted power measurements must be made at many random polarizations of the incoming light. The polarization may be changed by using a polarization controller (manual or electronic) or a scrambler, preferably with angled connections. The use of the scrambler requires knowledge of the scrambling speed (degree/s change on the Poincaré sphere, or highest frequency component in the scrambling instrument). The scrambling speed should be slow enough to guarantee that each power meter measurement is completed before there is significant polarization change. In other terms, the time employed by the scrambler to produce an appreciable polarization change must be longer than the power meter integration time, to avoid that the power variations induced by polarization scrambling are averaged-out by the power meter integration time. So, with a power meter integration time of 100 ms, a scrambling frequency of 5 Hz must be used, meaning that a substantial variation of the polarization takes place in 200 ms.

IV.3.2.2.2. Translation stage

The translation length must be set after the mode beating period has been determined, which should be done with the polarization scrambling turned off. The translation length should be chosen between a lower limit dictated by the periodicity of the mode beating (two periods is recommended) and an upper limit corresponding to an appropriate fibre strain. In the case of a two-metre cable sample, the lower limit of the translation length would be ~2 mm and the upper limit would be ~20 mm. The velocity of the translation stage must be slow enough to guarantee that the time employed for a complete peak/trough cycle is much longer than the power meter integration time, to avoid that the power oscillations induced by fibre length variation are averaged-out by the power meter integration time. As an example, a translation velocity of 0.2 mm/s would complete a peak/trough cycle of 1mm in 5 s, much longer than the power meter integration time of 100 ms.

IV.3.2.2.3. Sampling frequency

Once the power meter integration time, the speed of the scrambling, the translation stage velocity and its excursion have been set in accordance with the criteria exposed in the previous two points, the frequency of the power meter acquisitions must be decided. The sampling frequency should be high enough to guarantee a clear identification of the peak/trough cycle determined by the fibre stretching, with no less than 25 points collected for each oscillation period. However, the time distance between two consecutive acquisitions must be greater than the power meter integration time, to ensure that they correspond to truly different interference and polarization states. Namely, an acquisition every 200 ms would be compatible with the parameter values exemplified in the previous (a)-(b) points.

IV.3.2.2.4. Number of measurements

A reliable MPI evaluation can be obtained only if a large enough number of power meter readings, corresponding to a different polarization state of the injected light and phase differences between the co-propagating mode, are collected. With the suggested parameter values, a translation length of 4 mm, corresponding to 4 beating periods, would provide 100 power meter readings and would take 20 seconds. To assess the reliability of the resulting MPI value, this measurement should be repeated at least 20 times, so that in 400 seconds 20 different MPI values can be calculated, having collected a total of 2000 power meter readings corresponding to a different state of the injected light polarization and of the mode phase different. The average and the standard deviation of the collected MPI values provide a complete statistical description of the expected penalty.

IV.3.2.2.5. Using a manual polarization scrambler

If a manual scrambler is to be used, as a preliminary step it is necessary to test the light source – scrambler combination to verify that randomly distributed polarization states on the entire Poincaré sphere are obtained. In this case, instead of continuously scrambling the polarization while the fibre stretching takes place, it could be easier to change the polarization after every translation run. Assuming that 100 power meter acquisitions are made during each run, and that 20 runs are performed with 20 different polarization states, the MPI can be calculated on a total of 2000 power meter readings.

IV.3.2.3. Mode stripping loop

See clause IV.1.2.3.

IV.3.2.4. Optical receiver

See clause IV.1.2.4.

IV.3.3. Measurements procedure

IV.3.3.1. Preparation of the fibre under test

This test method employs an uncabled fibre jumper with offset fusion splices at the ends. The fibre is nominally 2 m in length and the splice losses must be individually characterized (see clause IV.1.3.3).

IV.3.3.2. Baseline measurement

Before including the test fibre in the measurement set-up, measure a baseline response by connecting the polarization scrambler and RX in Figure IV.3 with a 10 m long [ITU-T G.652] fibre and stretching 2 m of it without affecting the splice/connection loss.

IV.3.3.3. Insert short fibre test sample

The test fibre may be attached using paper tape to the translation stages. It is recommended that the fibre be straight, with the tape covering ~ 10 cm of fibre at either side of the fusion splice (covering the splice for protection). The fibre between the stages is usually ~2 m in length and under slight tension (straight).

IV.3.3.4. Short-cabled fibre measurement

With the light source and polarization scrambler active, the translation stage is moved in small increments. With each movement, the transmitted power is recorded along with the position of the stage. The stage movement must be sufficient to eventually allow exploration of two FSR of the test fibre (the transmitted power versus fibre length goes through two maxima and minima). At this point the stage reverses direction and more data is taken. This process continues until enough polarization states have been sampled (~100) at each fibre length. If desired, the light source wavelength can be slowly varied as well.

IV.3.3.5. Calculations

Find the MPI by determining the maximum and minimum power transmitted through the sample over all fibre stretch lengths and polarization states; then use the formula from Equation (IV-1), repeated below:

$$MPI(dB) = 20\log\left[\frac{10^{\mathrm{PR}/20} - 1}{10^{\mathrm{PR}/20} + 1}\right]$$

where PR is the difference between the maximum and minimum power levels detected (in dB). Note that if the photodetector/oscilloscope method is used, the output data is an electrical voltage, not an optical power. Due to the linearity of the photodetector, Equation (IV-1) can still be used with a voltage difference when voltages have been converted to dB (10 log V). Dark current corrections should be made prior to this conversion. Verify that the MPI, computed directly from the baseline data, is suitably low.

IV.3.3.6. Presentation of the results

See clause IV.1.3.6.

Appendix V

The interferometric technique for chromatic dispersion measurement

(This appendix does not form an integral part of this Recommendation.)

V.1. General

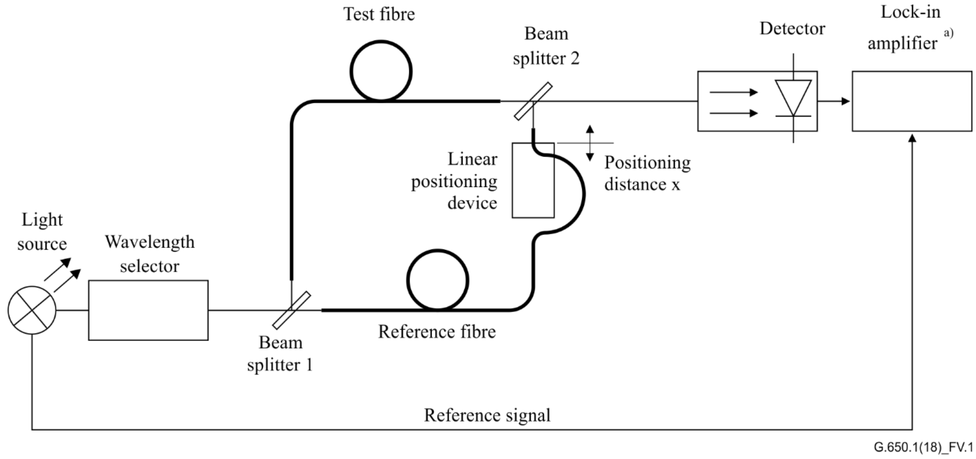
The interferometric test method allows the chromatic dispersion to be measured, using a short piece of fibre (several metres). This offers the possibility of measuring the longitudinal chromatic dispersion homogeneity of optical fibres. Moreover, it is possible to test the effect of overall or local influences, such as temperature changes and macrobending losses, on the chromatic dispersion.

According to the interferometric measuring principle, the wavelength-dependent time delay between the test sample and the reference path is measured by a Mach-Zehnder interferometer. The reference path can be an air path or a single-mode fibre with known spectral group delay.

It should be noted that extrapolation of the chromatic dispersion values derived from the interferometric test on fibres of a few metres length, to long fibre sections assumes longitudinal homogeneity of the fibre. This assumption may not be applicable in every case.

V.2. Test apparatus

Schematic diagrams of the test apparatus using a reference fibre and an air path reference are shown in Figure V.1 and Figure V.2, respectively.



a) When needed

Figure V.1 — Schematic diagram of measurement set-up with reference fibre

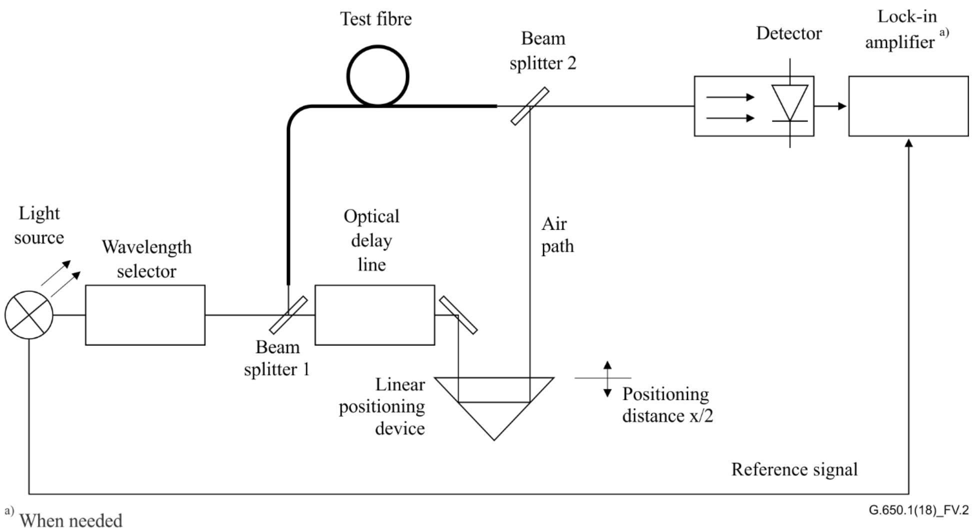


Figure V.2 — Schematic diagram of measurement set-up with air path reference

V.2.1. Optical source

The source should be stable in position, intensity and wavelength for a time period sufficiently long to complete the measurement procedure. The source must be suitable, e.g., a YAG laser with a Raman fibre or a lamp and LED optical sources, etc. For the application of lock-in amplification techniques, a light source with low-frequency modulation (50 to 500 Hz) is sufficient.

V.2.2. Wavelength selector

A wavelength selector is used to select the wavelength at which the group delay is measured. A monochromator, optical interference filter, or other wavelength selector may be used depending on the type of optical sources and measurement systems. The wavelength selector may be used either at the input or the output end of the fibre under test.

The spectral width of the optical sources is to be restricted by the dispersion measuring accuracy, and it is about 2 to 10 nm.

If a mathematical fit is made to the data, at least one data point must be within 100 nm of λ_0.

V.2.3. Optical detector

The optical detector must have a sufficient sensitivity in that wavelength range in which the chromatic dispersion has to be determined. If necessary, the received signal could be upgraded with, for example, a transimpedance circuit.

V.2.4. Test equipment

For the recording of the interference patterns, a lock-in amplifier may be used. Balancing of the optical length of the two paths of the interferometer is performed with one linear positioning device in the reference path. Concerning the positioning device, attention should be paid to the accuracy, uniformity and stability of linear motion. The variation of the length should cover the range from 20 to 100 mm with an accuracy of about 2 µm.

V.2.5. Specimen

The specimen for the test can be uncabled and cabled single-mode fibres. The length of the specimen should be in the range 1 m to 10 m. The accuracy of the length should be about ±l mm. The preparation of the fibre end faces should be carried out with reasonable care.

V.2.6. Data processing

For the analysis of the interference patterns, a computer with suitable software should be used.

V.3. Measurement procedure

1) The fibre under test is placed in the measurement set-up (Figure V.1 and Figure V.2). The positioning of the end faces is carried out with 3-dimensional micro-positioning devices by optimizing the optical power received by the detector. Errors arising from cladding modes are not possible.

2) The determination of the group delay is performed by balancing the optical lengths of the two interferometer paths with one linear positioning device in the reference path for different wavelengths. The difference between position x_i of the maximum of the interference pattern for wavelength λ_i and position x_0 for wavelength λ_0 (Figure V.3) determines the group delay difference $\Delta\tau_g(\lambda_i)$ between the reference path and the test path as follows:

$$\Delta\,\tau_g(\lambda_i) = \frac{x_0 - x_i}{c_0} \qquad \text{(V-1)}$$

where c_0 is the velocity of light in the vacuum. The group delay of the test sample is calculated by adding the value $\Delta\tau_g(\lambda_i)$ and the spectral group delay of the reference path. Dividing this sum by the test fibre length then gives the measured group delay difference per unit length $\tau(\lambda)$ of the test fibre.

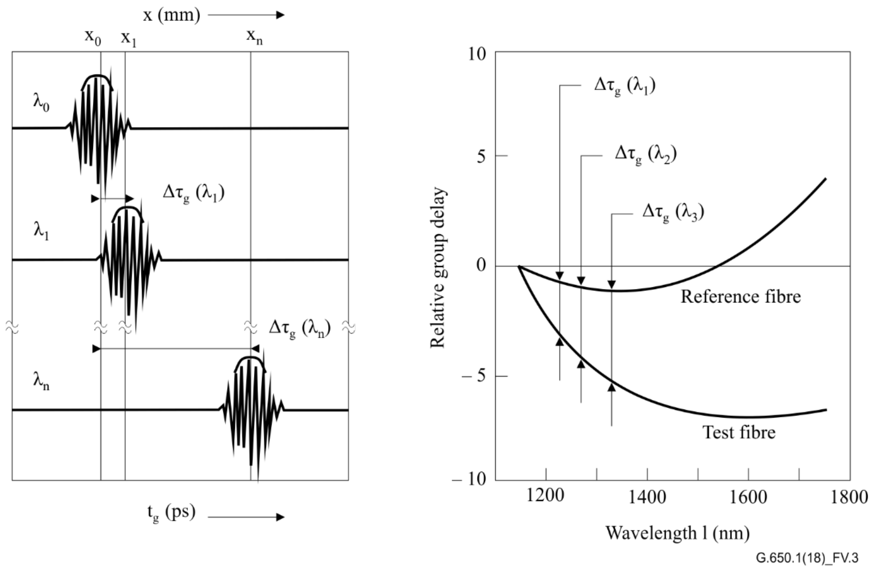


Figure V.3 — Determination of the spectral group delay

V.4. Presentation of the results

The following details shall be presented:

a) test set-up arrangement;
b) source characteristics;
c) fibre identification and length;
d) characteristics of the wavelength selector (if present);
e) type of photodetector;
f) model used to fit the relative group delay data or chromatic dispersion data, and the fitting wavelength range used;
g) values of coefficients from the fit for each fitting wavelength range;
h) temperature of the sample and environmental conditions (if necessary).

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